

Fan Zhou; Yanjun Shen; Zebin Wu

Non-fragile observers design for nonlinear systems with unknown Lipschitz constant

Kybernetika, Vol. 60 (2024), No. 4, 475–491

Persistent URL: <http://dml.cz/dmlcz/152615>

Terms of use:

© Institute of Information Theory and Automation AS CR, 2024

Institute of Mathematics of the Czech Academy of Sciences provides access to digitized documents strictly for personal use. Each copy of any part of this document must contain these *Terms of use*.



This document has been digitized, optimized for electronic delivery and stamped with digital signature within the project *DML-CZ: The Czech Digital Mathematics Library* <http://dml.cz>

NON-FRAGILE OBSERVERS DESIGN FOR NONLINEAR SYSTEMS WITH UNKNOWN LIPSCHITZ CONSTANT

FAN ZHOU, YANJUN SHEN, ZEBIN WU

In this paper, the problem of globally asymptotically stable non-fragile observer design is investigated for nonlinear systems with unknown Lipschitz constant. Firstly, a definition of globally asymptotically stable non-fragile observer is given for nonlinear systems. Then, an observer function of output is derived by an output filter, and a dynamic high-gain is constructed to deal with unknown Lipschitz constant. Even the observer gains contain diverse large disturbances, the observer errors are proven to converge to the origin based on Lyapunov stability theorem and a matrix inequality. Finally, an experimental simulation is provided to confirm the validity of the proposed method.

Keywords: non-fragile, observer, high gain, unknown Lipschitz constant, output filter

Classification: 93C10

1. INTRODUCTION

Since the concept of nonlinear system observer was first proposed in [27], numerous outcomes have been achieved [7, 10, 17]. In the area of observer design, one of the most difficult problems is how to deal with the nonlinear terms. Researchers often assume that the nonlinear terms satisfy the Lipschitz condition. But only few papers have discussed the observer design problem of nonlinear systems with unknown Lipschitz constant [12, 15, 23]. In addition, the unknown Lipschitz constant considered in the literature [23] required to meet some constraints. These observer design methods are all based on LMI (linear matrix inequality) technology.

The application of observer in secure communication has also been studied in [25, 18]. Its principle is to use the state observer to design a receiving system synchronized with the chaotic system, and modulate a digital signal to a certain parameter of the transmission system. At the receiving terminal, the signal is demodulated by using the synchronization error. Moreover, secure communication was also achieved by designing electronic circuits in [22].

It is reported that there often exist observer gain drifts in some industrial applications because of round-off errors in calculation or sensor devices aging [29]. Since a design method of non-fragile observers was firstly proposed in [14], more and more scholars begin to explore the observer design problem in the presence of observer gain disturbances.

For example, the authors in [29] introduced the following uncertainty linear system

$$\begin{aligned}\dot{x}(t) &= (A + D_1\Delta(t)E)x(t) + \omega_1(t), \\ y(t) &= (C + D_2\Delta(t)E)x(t) + \omega_2(t),\end{aligned}$$

where $\Delta(t)$ is a time-varying matrix of uncertain parameters and $\omega_1(t)$, $\omega_2(t)$ are two zero mean white Gaussian noises. An observer was constructed as

$$\dot{\xi}(t) = A\xi(t) + (G + \Delta G)y(t),$$

where G and ΔG denote the observer gain and the gain drift, respectively. Despite the gain drift ΔG is uncertain due to round-off error and sensor devices aging reasons, the estimation value $\xi(t)$ is still available. Based on an LMI optimization method, a non-fragile observer for nonlinear systems was proposed in [11]. By introducing adaptive technology, the authors in [13] designed an adaptive non-fragile observer. For switching systems, the H_∞ non-fragile observers were studied in [30]. For discrete switching systems, the non-fragile observers were also researched in [28]. However, all the above results are obtained based on the LMI technology.

Although the LMI conditions can be easily tested by computer. However, if the solvable conditions of LMI are not satisfied, the design methods will be failure. Therefore, for nonlinear systems with unknown Lipschitz constants, it is very important to find other methods to design non-fragile observers.

In [1, 2, 3, 8, 9, 20], the high-gain observer design method was proposed for nonlinear systems. The introduced high-gain enables that the observer errors are exponentially convergent. Moreover, the high-gain observers are always achievable. However, there is a blank area to design high-gain observers for nonlinear systems with unknown Lipschitz constant. Although the dynamic high-gain technique is investigated to deal with unknown Lipschitz constant in controller design [19, 21], it is worth of a further study on how to handle the unknown Lipschitz constant in observer design.

In this paper, the problem of non-fragile high-gain observer design is investigated for nonlinear systems with unknown Lipschitz constant. Based on a matrix inequality and a monotone non-decreasing dynamic gain, it is proven that the observer errors are globally asymptotically stable even if there are distinct large disturbances in the observer gains. The paper is structured as follows: Section 2 presents the problem formulation and some important lemmas. The design process of the non-fragile observers is presented for a class of lower triangular nonlinear systems in Section 3. In Section 4, a simulation example demonstrates the effectiveness of the designed method. Section 5 provides a conclusion to the full text.

2. PROBLEM FORMULATION AND PRELIMINARIES

2.1. Problem description

Consider the following nonlinear system

$$\begin{aligned}\dot{x}(t) &= A_0x(t) + B_0u(t) + f_0(x), \\ y(t) &= C_0x(t),\end{aligned}\tag{1}$$

where $A_0 = \begin{pmatrix} 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & 1 \\ 0 & 0 & \cdots & 0 \end{pmatrix}$, $B_0 = (0 \ 0 \ \cdots \ 1)^T$, $C_0 = (1 \ 0 \ \cdots \ 0)$.

$x(t)$ and $y(t)$ are the state variable and output variable, respectively. The nonlinear function vector $f_0(x) = (f_1(x_1^t), f_2(x_2^t), \dots, f_n(x_n^t))^T \in \mathbb{R}^n$, where $f_i(x_i^t) \in \mathbb{R}$ is a continuous nonlinear function, and $x_i^t = (x_1, \dots, x_i)^T$.

The following assumption is imposed on the nonlinear system (1).

Assumption 2.1. The nonlinear function vector $f_i(x_i^t)$ satisfies the following condition

$$|f_i(x_i^t) - f_i(\hat{x}_i^t)| \leq \varrho(|x_1(t) - \hat{x}_1(t)| + \cdots + |x_i(t) - \hat{x}_i(t)|), i = 1, \dots, n,$$

where $\varrho > 0$ is an unknown constant.

Remark 2.2. In order to explain the rationality of Assumption 2.1, introduce the following Duffing oscillator [5],

$$\begin{cases} \dot{x}_1(t) = x_2(t), \\ \dot{x}_2(t) = -a_0x_1(t) - c_0x_2(t) + x_1^3(t) + u(t), \\ y(t) = x_1(t), \end{cases} \tag{2}$$

where $u(t) = \sin t + \sqrt{2}$. According to [5], if we select $a_0 = c_0 = 5$, then the system (2) exists periodic solutions. However, the authors don't provide a specific expression of the periodic solutions or a boundary of the periodic solutions. That is, the nonlinear term $x_1^3(t)$ satisfies the Lipschitz condition with an unknown Lipschitz constant.

We need the following definition.

Definition 2.3. (Jeong et al. [14]) For nonlinear system (1), construct an observer as,

$$\begin{aligned} \dot{\hat{x}}(t) &= A_0\hat{x}(t) + B_0u(t) + \Omega_0 \cdot \Delta\Omega_0\varphi(y, \hat{y}) + f(\hat{x}), \\ \hat{y}(t) &= C_0\hat{x}(t), \end{aligned} \tag{3}$$

where $\varphi(y, \hat{y})$ is an observer function, $\Omega_0 = \text{diag}\{g_1, \dots, g_n\}$ is the observer gain, $\Delta\Omega_0 = (\Delta g_1, \dots, \Delta g_n)^T$ is unknown multiplicative disturbance arising by electronic components aging or round-off errors in calculation [29].

If there exists two constants g_{\max} and g_{\min} that satisfy $g_{\min} < \Delta g_i < g_{\max}, i = 1, \dots, n, \forall x(t_0) \in \mathbb{R}^n$ and $\hat{x}(t_0) \in \mathbb{R}^n$, we have

$$\lim_{t \rightarrow \infty} (x_i(t) - \hat{x}_i(t)) = 0, i = 1, \dots, n. \tag{4}$$

Then the system (3) is a globally asymptotically stable non-fragile observer of nonlinear system (1).

Remark 2.4. There are various design methods for the observer function $\varphi(y, \hat{y})$ in (3). For example, we can directly select $\varphi(y, \hat{y}) = y - \hat{y}$ to build nonlinear robust observer [4]. In [6], the observer function is selected as $\varphi_i(y, \hat{y}) = L^i(y - \hat{y})$ (L is the high-gain

parameter) to establish the high-gain observer. A dynamic high-gain observer is designed by selecting $\varphi_i(y, \hat{y}) = L^i(t)(y - \hat{y})$ ($L(t)$ is the dynamic high-gain function) in [19]. In order to design a finite-time observer, one can choose $\varphi_i(y, \hat{y}) = |y - \hat{y}|^{\alpha_i} \text{sign}(y - \hat{y})$ ($\alpha_i \in (0, 1)$) [26]. In this article, we investigate that how to select the appropriate observer function $\varphi(y, \hat{y})$ to design globally asymptotically stable non-fragile high-gain observer for the nonlinear system (1).

Remark 2.5. In order for demonstrating the observer gain sensitivity, introduce the following nonlinear system as an example,

$$\begin{aligned} \dot{x} &= A^*x + B^*u + F^*(x), \\ y &= C^*x, \end{aligned}$$

where $A^* = \begin{pmatrix} 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 \end{pmatrix}$, $B^* = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 1 \end{pmatrix}$, $F^*(x) = \begin{pmatrix} 0 \\ 0 \\ 2x_4 \\ 9x_5 + \cos(x_4) \\ x_5 \sin(x_5) \end{pmatrix}$

and $C^* = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 \end{pmatrix}$.

Design an observer for the nonlinear system,

$$\begin{aligned} \dot{\hat{x}} &= A^*\hat{x} + B^*u + F^*(\hat{x}) + \kappa C^*(x - \hat{x}) \\ \hat{y} &= C^*\hat{x}, \end{aligned}$$

where the observer gain $\kappa = (53.6 \ 241.6 \ 320.6 \ 13.1 \ 34.6)^T$.

Next, by letting $e = x - \hat{x}$, the error system becomes,

$$\dot{e} = A_{\kappa}e + F^*(e),$$

where $A_{\kappa} = A^* - \kappa C^*$ and $F^*(e) = F^*(x) - F^*(\hat{x})$. Assumethe initial state $(x_1, x_2, x_3, x_4, x_5) = (3, 1, 2, 3, 2)$ and $(\hat{x}_1, \hat{x}_2, \hat{x}_3, \hat{x}_4, \hat{x}_5) = (-4, -1, 2, 1, 1)$, and the simulation results are shown in Fig. 1. Obviously, the simulation result shows the error system is stable.

However, if there exists a small disturbance $\Delta = (0.1 \ 0.1 \ 0.1 \ 0.1 \ 0.1)^T$ in the observer gain, then the new error system $\varpi = x - \hat{x}$ becomes,

$$\dot{\varpi} = A_{\Delta\kappa}\varpi + F^*(\varpi),$$

where $A_{\Delta\kappa} = A^* - (\kappa + \Delta)C^*$ and $F^*(\varpi) = F^*(x) - F^*(\hat{x})$. The simulation is presented in Fig. 2. It reveals the error system is unstable. Moreover, we have $\frac{\|\Delta\|}{\|\kappa\|} = 0.00075301$, which indicates the error system is very fragile with respect to the observer gain disturbance.

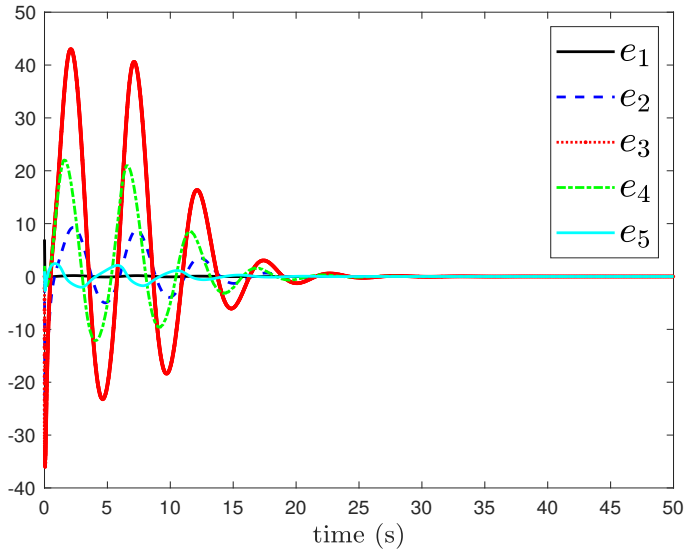


Fig. 1. The trajectories of the estimation error e .

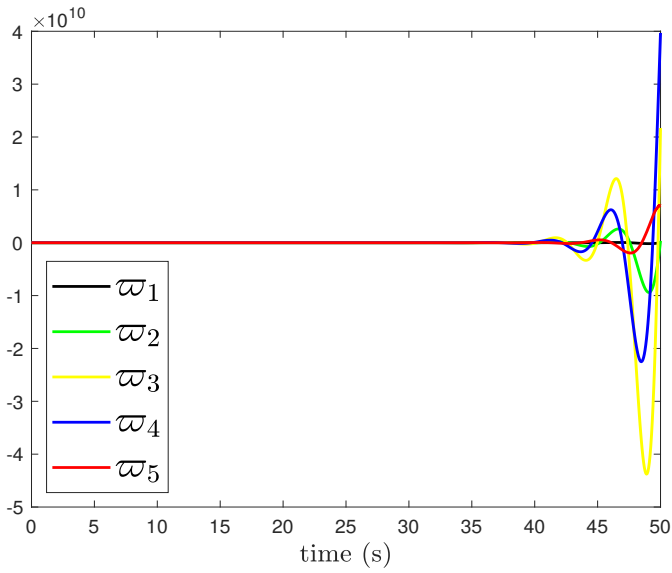


Fig. 2. The trajectories of the estimation error w .

Remark 2.6. Due to the augmented system (7) does not preserve the strict triangular form, it is necessary to figure out whether the augmented system (7) is observable. The observable matrix can be calculated as

$$\begin{pmatrix} C_1 \\ C_1 A_1 \\ \vdots \\ C_1 A_1^{n-1} \end{pmatrix} = \begin{pmatrix} 1 & 0 & \cdots & 0 \\ L(t)\kappa_0 & 1 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ L^n(t)\kappa_0^n & L^{n-1}(t)\kappa_0^{n-1} & \cdots & 1 \end{pmatrix}.$$

Obviously, the rank of the observable matrix is $n + 1$. Therefore, the augmented system (7) is observable.

Our aim is to design a globally asymptotically stable non-fragile high-gain observer for the nonlinear system (7). That is, the designed observer gains $\kappa_1, \dots, \kappa_n$ are negative and have unknown observer gain disturbances $\theta_i(t)$, $i = 1, \dots, n$, which are continuous and satisfy the following conditions

$$\begin{aligned} 0 < \theta_i^{\min} \leq 1, \\ 1 \leq \theta_i^{\max} < +\infty, \\ \theta_i^{\min} \leq \theta_i(t) \leq \theta_i^{\max}, \end{aligned} \tag{5}$$

where θ_i^{\min} and θ_i^{\max} are some positive constants.

Remark 2.7. Normally, the observer gain disturbances Δg_i , $i = 1, \dots, n$ have additive form and multiplicative form. The additive form is able to transform to the multiplicative form by the transformation $g_i + \Delta g_i = g_i(1 + \frac{1}{g_i}\Delta g_i)$. The multiplicative form is also able to transform to the additive form by the transformation $g_i\Delta g_i = g_i + g_i(\Delta g_i - 1)$. We are going to consider the multiplicative form in this paper.

2.2. Important lemmas

Lemma 2.8. Barbalat’s lemma [24]: For $t \geq t_0$ ($t_0 \in \mathbb{R}^+$), if $\Phi(t)$ is uniformly continuous and $\int_{t_0}^t \Phi(t) dt$ is bounded when $t \rightarrow \infty$, then

$$\lim_{t \rightarrow +\infty} \Phi(t) = 0.$$

For the convenience of presentation, the definitions of some parameters are provided for later use.

- 1) Choose the positive constants b_j , $j = 2, \dots, n + 1$, such that,

$$\begin{aligned} (n^2 \prod_{k=2}^j b_k^2 \max\{(\eta_i^{\max} - \eta_{i-1}^{\min})^2, (\eta_{i-1}^{\max} - \eta_i^{\min})^2\})(\alpha_1(\cdot) + \alpha_2(\cdot) + \alpha_3(\cdot)) < 1, \\ j = 2, \dots, n + 1, \end{aligned}$$

where

$$\begin{aligned} 0 < \eta_i^{\min} \leq 1, \\ 1 \leq \eta_i^{\max} < +\infty, \\ \eta_1^{\max} = \eta_1^{\min} = 1, \end{aligned}$$

and

$$\begin{aligned} \alpha_1(\cdot) &= \left(\frac{\beta_2(\cdot)}{b_2} + 2\beta_3(\cdot)b_2\right)^2 \max\{(\eta_n^{\max} - 1)^2, (1 - \eta_n^{\min})^2\}, \\ \alpha_2(\cdot) &= 2 \sum_{i=3}^{n+1} (\prod_{k=3}^i b_k^2 \left(\frac{\beta_2(\cdot)}{b_2} + 2\beta_i(\cdot)b_2\right)^2 \max\{(\eta_i^{\max} - \eta_{i-1}^{\min})^2, (\eta_{i-1}^{\max} - \eta_i^{\min})^2\}), \\ \alpha_3(\cdot) &= 8 \sum_{i=3}^{n+1} (\prod_{k=2}^i b_k^2 (\beta_i(\cdot) - \beta_{i+1}(\cdot))^2 \max\{(\eta_i^{\max} - 1)^2, (1 - \eta_i^{\min})^2\}), \end{aligned}$$

where $\beta_i(b_{i+1}, \dots, b_{n+1}) = \frac{b_i a_{i-1}}{2k_0 a_i}$, $i = 1, \dots, n + 1$ satisfies $\beta_{n+1}(\cdot) = 1$ and $\beta_{n+2}(\cdot) = 0$.

2) The positive constants a_j , $j = 1, \dots, n + 1$, can be calculated by,

$$\begin{aligned} a_n &= \frac{2a_{n+1}}{b_{n+1}} k_0, \\ a_{i-1} &= \frac{2a_i}{b_i} \left(k_0 + \frac{ia_i}{2a_{i+1}} b_{i+1} + \frac{ia_i}{2a_{i+1} b_{i+1}} + \frac{1}{2} \sum_{j=i}^n \left(\left(\frac{b_{j+2} a_{j+1}}{a_{j+2}} + \frac{j b_{j+1} a_j}{a_{j+1}}\right) \prod_{k=i+1}^{j+1} b_k^2\right)\right), \\ i &= 2, \dots, n, \end{aligned}$$

where $a_{n+2} = 1$, $b_{n+2} = 0$, k_0 and a_{n+1} are arbitrary positive constants.

3) The gains k_i , $i = 1, \dots, n + 1$, can be calculated by,

$$\begin{aligned} k_1 &= -b_2 \frac{a_1}{a_2} - \frac{a_1}{2b_2 a_2} - \alpha_0 k_0, \\ k_i &= \frac{a_1}{a_i} \left(\frac{a_{i-1}}{a_1} b_i k_{i-1} + \frac{a_{i-1}}{a_i} b_i \prod_{k=2}^i b_k - \frac{a_i}{a_{i+1}} \prod_{k=2}^i b_k\right), \quad i = 2, \dots, n + 1. \end{aligned}$$

4) Let

$$A_2 = \begin{pmatrix} k_1 & 1 & 0 & \cdots & 0 \\ k_2 \eta_2(t) & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ k_n \eta_n(t) & 0 & 0 & \cdots & 1 \\ k_{n+1} \eta_{n+1}(t) & 0 & 0 & \cdots & 0 \end{pmatrix},$$

and

$$P_0 = \begin{pmatrix} a_1 & 0 & 0 & \cdots & 0 & 0 \\ -b_2 a_1 & a_2 & 0 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & a_n & 0 \\ 0 & 0 & 0 & \cdots & -b_{n+1} a_n & a_{n+1} \end{pmatrix},$$

where $\eta_i^{\min} \leq \eta_i(t) \leq \eta_i^{\max}$.

The positive definite matrix $\Gamma(\eta(t))$ is produced by

$$\begin{aligned} \Gamma_{1,1}(\eta(t)) &= \alpha_0 k_0, \\ \Gamma_{1,i}(\eta(t)) &= \Gamma_{i,1}(\eta(t)) = (1 - \eta_i(t)) \left(\frac{a_{i-1}}{a_i} b_i \prod_{k=2}^i b_k - \frac{a_i}{a_{i+1}} \prod_{k=2}^{i+1} b_k\right) \\ &\quad + (\eta_i(t) - \eta_{i-1}(t)) \left(\frac{a_1}{2b_2 a_2} \prod_{k=2}^i b_k + \frac{a_{i-1}}{a_i} b_i \prod_{k=2}^i b_k\right), \\ \Gamma_{i,i}(\eta(t)) &= k_0, \\ \Gamma_{i,j}(\eta(t)) &= 0, \quad i \neq j, \quad i = 2, \dots, n + 1, \quad j = 2, \dots, n + 1, \end{aligned}$$

where $\Gamma_{i,j}(\eta(t))$ means the i th line and the j th column element of the matrix $\Gamma(\eta(t))$.

From [16], for the matrices A_2 , P_0 and $\Gamma(\eta(t))$ defined above, the following lemma can be indicated.

Lemma 2.9. (Koo and Choi [16]) There exists a positive constant λ_0 satisfying

$$A_2^T P + P A_2 = -P_0^T \Gamma(\eta(t)) P_0 \leq -\lambda_0 I,$$

where $P = P_0^T P_0$.

For the positive definite matrix P , the following result can be obtained.

Lemma 2.10. For the matrix $Q = \begin{pmatrix} \sigma & 0 & 0 & \cdots & 0 \\ 0 & 1 + \sigma & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & n + \sigma \end{pmatrix}$, where σ denotes

a positive constant. There exists a positive constant $\bar{\sigma}$ such that when $\bar{\sigma} < \sigma$, the following matrix inequality holds,

$$PQ + QP > 0.$$

Proof. For the system $\dot{\xi} = Q\xi$, introduce the transformation $\psi = P_0\xi$. Then,

$$\begin{aligned} \dot{\psi}_1 &= \sigma\psi, \\ \dot{\psi}_i &= -b_i a_{i-1} (i - 2 + \sigma) \left(\frac{\psi_{i-1}}{a_{i-1}} + \frac{1}{a_{i-1}} \sum_{j=1}^{i-2} \psi_j \Pi_{k=j+1}^{i-1} b_k \right) \\ &\quad + a_i (i - 1 + \sigma) \left(\frac{\psi_i}{a_i} + \frac{1}{a_i} \sum_{j=1}^{i-1} \psi_j \Pi_{k=j+1}^i b_k \right), \\ &= (i - 1 + \sigma)\psi_i - (i - 2 + \sigma) \sum_{j=1}^{i-1} \psi_j \Pi_{k=j+1}^i b_k + (i - 1 + \sigma) \sum_{j=1}^{i-1} \psi_j \Pi_{k=j+1}^{i-1} b_k, \\ &= (i - 1 + \sigma)\psi_i + \sum_{j=1}^{i-1} \psi_j \Pi_{k=j+1}^i b_k, \quad i = 2, \dots, n + 1. \end{aligned}$$

Thus, there exists a positive real $\bar{\sigma}$ such that when $\sigma > \bar{\sigma}$, the following inequality holds.

$$\begin{aligned} \sum_{i=1}^{n+1} \psi_i \dot{\psi}_i &= \sum_{i=1}^{n+1} (i - 1 + \sigma)\psi_i^2 + \sum_{i=1}^{n+1} \psi_i \sum_{j=1}^{i-1} \psi_j \Pi_{k=j+1}^i b_k \\ &\geq \sum_{i=1}^{n+1} (\sigma - \bar{\sigma})\psi_i^2 > 0. \end{aligned}$$

Therefore,

$$\sum_{i=1}^{n+1} \psi_i \dot{\psi}_i = \frac{1}{2} \frac{d(\psi^T \psi)}{dt} = \frac{1}{2} \xi^T (QP + PQ)\xi > 0.$$

The proof is completed. □

3. THE NON-FRAGILE OBSERVER DESIGN

Consider the following transformation,

$$\dot{\tilde{x}}_0(t) = L(t)\kappa_0\bar{x}_0(t) + y(t), \tag{6}$$

where $L(t)$ is a time-varying function to be designed and κ_0 is a negative constant. Thus, the nonlinear system (1) can be augmented as,

$$\begin{aligned} \dot{\tilde{x}}(t) &= A_1\bar{x}(t) + B_1u(t) + f(\bar{x}), \\ \bar{y}(t) &= C_1\bar{x}(t), \end{aligned} \tag{7}$$

where $\bar{x}(t) = (\bar{x}_0, x_1, \dots, x_n)^T$, $A_1 = \begin{pmatrix} L(t)\kappa_0 & C_0 \\ 0_{n \times 1} & A_0 \end{pmatrix}$; $B_1 = \begin{pmatrix} 0_{1 \times 1} \\ B_0 \end{pmatrix}$, $C_1 = (C_0 \ 0_{1 \times 1})$ and $f(\bar{x}) = \begin{pmatrix} 0_{1 \times 1} \\ f_0(x) \end{pmatrix}$.

Then, the problem of non-fragile observer design for the nonlinear system (1) is transformed into observer design for the augmented nonlinear system (7) with multiplicative gain disturbances. The specific form is as follows.

$$\begin{aligned} \dot{\hat{x}}(t) &= A_1\hat{x}(t) + B_1u(t) + \Omega(\bar{y}(t) - \hat{x}_0(t)) + f(\hat{x}), \\ \hat{y}(t) &= C_1\hat{x}(t), \end{aligned} \tag{8}$$

where $\hat{x}(t)$ and $\hat{y}(t)$ are the estimation value of $\bar{x}(t)$ and $\bar{y}(t)$, respectively.

$$\Omega = \begin{pmatrix} 0 \\ -L^2(t)\kappa_1\theta_1(t) \\ \vdots \\ -L^{n+1}(t)\kappa_n\theta_n(t) \end{pmatrix}, \quad L(t) \text{ is the dynamic high-gain.}$$

$\kappa_i = k_{n+1-i}$, ($i = 0, \dots, n + 1$) are the observer gains and $\theta_i(t) = \eta_{n+1-i}(t)$, ($i = 1, \dots, n$) are the observer gain disturbances. Note that $\theta_i(t)$, $i = 1, \dots, n$, are continuous functions and satisfy

$$\begin{aligned} 0 &< \theta_i^{\min} \leq 1, \\ 1 &\leq \theta_i^{\max} < +\infty, \\ \theta_i^{\min} &\leq \theta_i(t) \leq \theta_i^{\max}, \end{aligned} \tag{9}$$

where θ_i^{\min} and θ_i^{\max} are positive constants. The dynamic high-gain $L(t)$ is selected as,

$$\dot{L}(t) = \left(\frac{\bar{y}(t) - \hat{x}_0(t)}{L^\sigma(t)}\right)^2, \quad L(t_0) = 1. \tag{10}$$

The dynamic high-gain $L(t)$ has the following property.

Proposition 3.1. If Assumption 2.1 holds, then the dynamic high-gain $L(t)$ defined in (10) is bounded for all $t \in [0, +\infty)$.

Proof.

Consider the following coordinates transformation,

$$\zeta_i(t) = \frac{\bar{x}_i(t) - \hat{x}_i(t)}{L^{i+\sigma}(t)}, \quad i = 0, \dots, n. \tag{11}$$

Therefore, from (7), (8), (11), we can deduce

$$\begin{aligned} \dot{\zeta}_0(t) &= L(t)\kappa_0\zeta_0(t) + L(t)\zeta_1(t) - \sigma \frac{\dot{L}(t)}{L(t)}\zeta_0(t), \\ \dot{\zeta}_i(t) &= L(t)\theta_i(t)\kappa_i\zeta_0(t) + L(t)\zeta_{i+1}(t) + \frac{1}{L^{i+\sigma}(t)}(f_i(x_i^t) - f_i(\hat{x}_i^t)) - (\sigma + i) \frac{\dot{L}(t)}{L(t)}\zeta_i(t), \\ &\hspace{15em} i = 1, \dots, n - 1, \\ \dot{\zeta}_n(t) &= L(t)\theta_n(t)\kappa_n\zeta_0(t) + \frac{1}{L^{n+\sigma}(t)}(f_n(x_n^t) - f_n(\hat{x}_n^t)) - (\sigma + n) \frac{\dot{L}(t)}{L(t)}\zeta_n(t), \end{aligned} \tag{12}$$

By representing (12) in compact form, it becomes

$$\dot{\zeta}(t) = L(t)A\zeta(t) + \tilde{f}(\tilde{x}) - \frac{\dot{L}(t)}{L(t)}Q\zeta(t), \tag{13}$$

where $A = \begin{pmatrix} \kappa_0 & 1 & 0 & \cdots & 0 \\ \kappa_1\theta_1(t) & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ \kappa_n\theta_n(t) & 0 & 0 & \cdots & 0 \end{pmatrix}$, $\tilde{f}(t, \tilde{x}) = \begin{pmatrix} 0 \\ \frac{1}{L^{1+\sigma}(t)}(f_1(x_1^t) - f_1(\hat{x}_1^t)) \\ \vdots \\ \frac{1}{L^{n+\sigma}(t)}(f_n(x_n^t) - f_n(\hat{x}_n^t)) \end{pmatrix}$ and

$$Q = \begin{pmatrix} \sigma & 0 & 0 & \cdots & 0 \\ 0 & 1 + \sigma & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & n + \sigma \end{pmatrix}.$$

Construct the Lyapunov function $V_1(t) = \zeta^T(t)P\zeta(t)$, and calculate it's derivative along the error system (13). Then, from Lemma 2.9 and Lemma 2.10, it becomes

$$\begin{aligned} \dot{V}_1(t) &= L(t)\zeta^T(t)(A^T P + PA)\zeta(t) + 2\zeta^T(t)P\tilde{f}(\tilde{x}) - \frac{\dot{L}(t)}{L(t)}\zeta^T(t)(PQ + QP)\zeta(t) \\ &\leq -L(t)\lambda_0\|\zeta(t)\|^2 + 2\zeta^T(t)P\tilde{f}(\tilde{x}). \end{aligned} \tag{14}$$

From Assumption 2.1, it follows that

$$2\zeta^T(t)P\tilde{f}(\tilde{x}) \leq \|\zeta(t)\|^2 + n^2\varrho^2\|P\|^2\|\zeta(t)\|^2. \tag{15}$$

Substituting (15) into (14) yields

$$\dot{V}_1(t) \leq -(L(t)\lambda_0 - 1 - n^2\varrho^2\|P\|^2)\|\zeta(t)\|^2. \tag{16}$$

Now, we prove the boundedness of $L(t)$ on $[0, t_f]$ by contradiction. Assume that $L(t)$ is not bounded on the interval $[0, t_f]$. Then,

$$\limsup_{t \rightarrow t_f} L(t) = +\infty. \tag{17}$$

Note that $L(t)$ is a monotone nondecreasing function. Then from (17), there exists $t_1 > 0$ such that $L(t)\lambda_0 - 1 - n^2\varrho^2\|P\|^2 > 1, \forall t \in [t_1, t_f]$.

Thus, from the differential inequality (16), we can infer that

$$\dot{V}_1(t) \leq -\|\zeta(t)\|^2, \forall t \in [t_1, t_f].$$

From (10), it follows that

$$\dot{L}(t) = \left(\frac{\bar{y}(t) - \hat{x}_0(t)}{L^\sigma(t)}\right)^2 \leq \|\zeta_0(t)\|^2 \leq \|\zeta(t)\|^2. \tag{18}$$

Therefore, from (17) and (18), the following conclusion can be drawn

$$+\infty = L(t_f) - L(t_1) = \int_{t_1}^{t_f} \dot{L}(t) dt \leq \int_{t_1}^{t_f} \|\zeta(t)\|^2 dt \leq V_1(\|\zeta(t_1)\|),$$

which is impossible. It reveals the dynamic gain $L(t)$ is bounded on $[t_1, t_f]$ and $\lim_{t \rightarrow t_f} L(t)$ is finite. The proof is completed. \square

Now, we give our main results.

Theorem 3.2. For the nonlinear system (1), if the observer gain disturbances $\theta_i(t)$ satisfy (9), then the system (6)–(8) is a globally asymptotically stable non-fragile observer of the nonlinear system (1), that is, $\forall x_i(t_0) \in \mathbb{R}$ and $\hat{x}_i(t_0) \in \mathbb{R}$,

$$\lim_{t \rightarrow \infty} (x_i(t) - \hat{x}_i(t)) = 0, \quad i = 1, \dots, n.$$

Proof. Since $\lim_{t \rightarrow t_f} L(t)$ is finite, there exists a constant \bar{L} such that

$$\bar{L} > \max\left\{\frac{n^2 \varrho^2 \|P\|^2 + 1 + 2\|P\|}{\lambda_0}, L(t)\right\}.$$

Introduce the coordinates transformation as follows,

$$z_i(t) = \frac{\bar{x}_i(t) - \hat{x}_i(t)}{\bar{L}^i}, \quad i = 0, \dots, n.$$

Thus, the error system becomes

$$\dot{z}(t) = \bar{L}Az(t) + \tilde{g}(\tilde{x}) + \bar{L}\Omega_1(t)z_0(t) - \bar{L}\Omega_2(t)z_0(t),$$

where $\tilde{g}(\tilde{x}) = \begin{pmatrix} 0 \\ \frac{1}{\bar{L}}(f_1(x_1^t) - f_1(\hat{x}_1^t)) \\ \vdots \\ \frac{1}{\bar{L}^n}(f_n(x_n^t) - f_n(\hat{x}_n^t)) \end{pmatrix}$, $\Omega_1(t) = \begin{pmatrix} \frac{L(t)}{\bar{L}}\kappa_0 \\ \frac{L^2(t)}{\bar{L}^2}\kappa_1\theta_1(t) \\ \vdots \\ \frac{L^{n+1}(t)}{\bar{L}^{n+1}}\kappa_n\theta_n(t) \end{pmatrix}$ and

$$\Omega_2(t) = \begin{pmatrix} \kappa_0 \\ \kappa_1\theta_1(t) \\ \vdots \\ \kappa_n\theta_n(t) \end{pmatrix}.$$

Design the Lyapunov function $V_2(t) = z^T(t)Pz(t)$. It is easy to find out

$$\begin{aligned} \dot{V}_2(t) &= \bar{L}z^T(t)(A^T P + PA)z(t) + 2z^T(t)P\tilde{g}(\tilde{x}) \\ &\quad + 2\bar{L}z^T(t)P\Omega_1(t)z_0(t) - 2\bar{L}z^T(t)P\Omega_2(t)z_0(t). \end{aligned} \tag{19}$$

By Assumption 2.1 and Lemma 2.9, it follows that

$$\begin{aligned} 2z^T(t)P\tilde{g}(\tilde{x}) &\leq \|z(t)\|^2 + n^2\varrho^2\|P\|^2\|z(t)\|^2 \\ 2\bar{L}z^T(t)P\Omega_1(t)z_0(t) &\leq \|P\|\|z(t)\|^2 + \bar{L}^2\|\Omega_1(t)\|^2z_0^2(t) \\ -2\bar{L}z^T(t)P\Omega_2(t)z_0(t) &\leq \|P\|\|z(t)\|^2 + \bar{L}^2\|\Omega_2(t)\|^2z_0^2(t) \end{aligned} \tag{20}$$

Substituting (20) into (19) yields

$$\begin{aligned} \dot{V}_2(t) &\leq -\bar{L}\lambda_0\|z(t)\|^2 + \|z(t)\|^2 + n^2\varrho^2\|P\|^2\|z(t)\|^2 \\ &\quad + 2\|P\|\|z(t)\|^2 + \bar{L}^2\|\Omega_1(t)\|^2z_0^2(t) + \bar{L}^2\|\Omega_2(t)\|^2z_0^2(t) \\ &\leq -c_0\|z(t)\|^2 + 2\bar{L}^{2+2\sigma}\bar{\Omega}^2\dot{L}(t), \end{aligned} \tag{21}$$

where $c_0 = \bar{L}\lambda_0 - 1 - n^2\varrho^2\|P\|^2 - 2\|P\| > 0$ and $\bar{\Omega} \geq \|\Omega_2(t)\| \geq \|\Omega_1(t)\|$.

Let λ_P is the minimum eigenvalue of matrix P , then

$$\lambda_P\|z(t)\|^2 - z^T(0)Pz(0) \leq -c_0 \int_{t_0}^t \|z(t)\|^2 dt + 2\bar{L}^{3+2\sigma}\bar{\Omega}^2L(t).$$

Since $L(t)$ is bounded on $[t_0, t_f)$, we can imply

$$\|z(t)\|^2 \leq \frac{z^T(0)Pz(0) + 2\bar{L}^{3+2\sigma}\bar{\Omega}^2L(t)}{\lambda_P}, \tag{22}$$

and

$$c_0 \int_{t_0}^t \|z(t)\|^2 dt \leq z^T(0)Pz(0) + 2\bar{L}^{3+2\sigma}\bar{\Omega}^2L(t). \tag{23}$$

Obviously, from (22) and (23), $\|z(t)\|$ is bounded on $[0, t_f)$ and $\int_{t_0}^t \|z(t)\| dt \leq +\infty$. By Lemma 2.8, we can conclude that $\lim_{t \rightarrow +\infty} \|z(t)\| = 0$, which completes the proof. \square

4. EXPERIMENTAL SIMULATIONS

In order to demonstrate the performance of the non-fragile observer, an experimental simulation is given in this section.

For the Duffing oscillator (2) mentioned in [5], by inserting an output filter, it becomes

$$\begin{cases} \dot{\hat{x}}_0(t) = \bar{x}_1(t) + L(t)\kappa_0\bar{x}_0(t), \\ \dot{\hat{x}}_1(t) = \bar{x}_2(t), \\ \dot{\hat{x}}_2(t) = -5\bar{x}_1(t) - 5\bar{x}_2(t) + \bar{x}_1^3(t) + u(t), \\ \bar{y}(t) = \bar{x}_0(t). \end{cases} \tag{24}$$

A globally asymptotically stable non-fragile observer can be designed as,

$$\begin{cases} \dot{\hat{x}}_0(t) = \hat{x}_1(t) + L(t)\kappa_0\hat{x}_0(t), \\ \dot{\hat{x}}_1(t) = \hat{x}_2(t) - L^2(t)\kappa_1\theta_1(t)(\bar{y}(t) - \hat{x}_0(t)), \\ \dot{\hat{x}}_2(t) = -5\hat{x}_1(t) - 5\hat{x}_2(t) + \hat{x}_1^3(t) + u(t) - L^3(t)\kappa_2\theta_2(t)(\bar{y}(t) - \hat{x}_0(t)), \\ \dot{L}(t) = \left(\frac{\bar{y}(t) - \hat{x}_0(t)}{L(t)}\right)^2, \\ \hat{y}(t) = \hat{x}_0(t). \end{cases} \tag{25}$$

Choose the initial states as $\bar{x}(0) = (3, -15, 18)^T$, $\hat{x}(0) = (0, 0, 0)^T$ and select $b_2 = 1$, $b_3 = 0.8$, $a_3 = k_0 = 1$. By Lemma 2, the observer gain vector can be obtained as $\kappa = (-25, -185, -319)$. Let $\theta_1(t) = 1.1 + 0.2 \sin t$, $\theta_2(t) = 0.9 + 0.5 \cos t$. The simulation results are shown in Fig. 3.

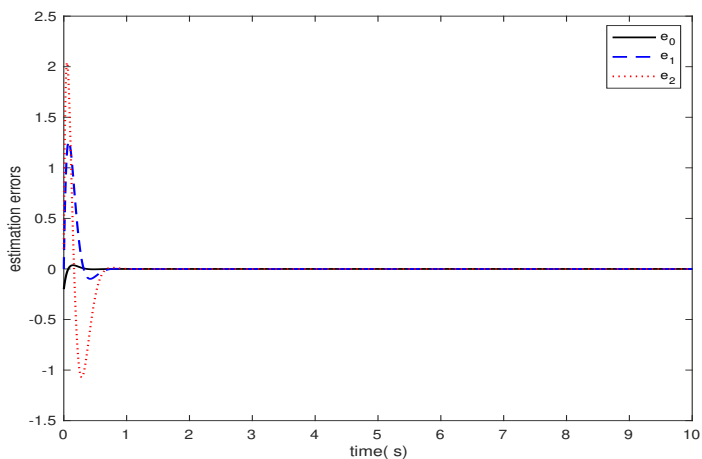


Fig. 3. The trajectories of the estimation errors.

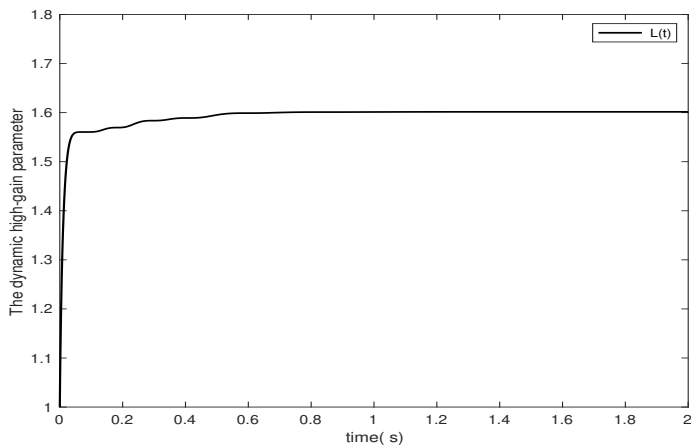


Fig. 4. The trajectory of the dynamic high-gain $L(t)$.

Fig. 4 shows the trajectory of the dynamic high-gain parameter $L(t)$. Obviously, the observer errors asymptotically converge to the origin and the dynamic high-gain is bounded.

In order to demonstrate the superiority of the non-fragile observer, we assume the Lipschitz constant is known. Then, plot a comparison figure with both the non-fragile observer and the following normal high-gain observer,

$$\begin{cases} \dot{\hat{x}}_0(t) = \hat{x}_1(t) + L\hat{x}_0(t), \\ \dot{\hat{x}}_1(t) = \hat{x}_2(t) - L^2\theta_1(t)(\bar{y}(t) - \hat{x}_0(t)), \\ \dot{\hat{x}}_2(t) = -5\hat{x}_1(t) - 5\hat{x}_2(t) + \hat{x}_1^3(t) + u(t) - L^3\theta_2(t)(\bar{y}(t) - \hat{x}_0(t)), \\ \hat{y}(t) = \hat{x}_0(t), \end{cases} \quad (26)$$

where $L = 10$ and other parameters keep fixed. Fig. 5 illustrates that our observer design method has better performance.

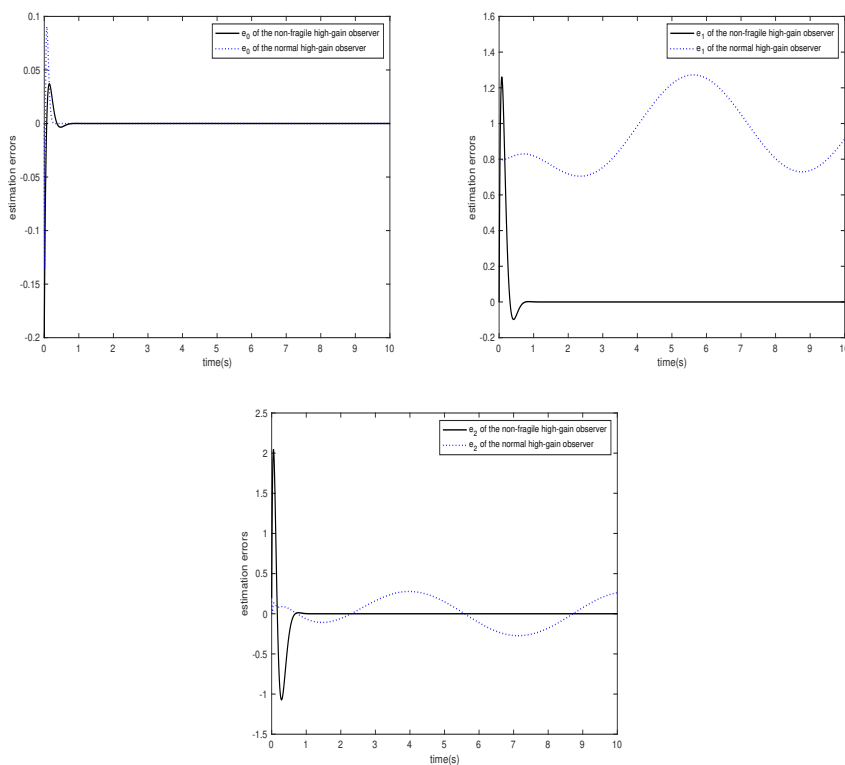


Fig. 5. The comparison between the non-fragile observer and the normal high-gain observer.

5. CONCLUSION

In this paper, we proposed a globally asymptotically stable non-fragile observer for nonlinear systems with unknown Lipschitz constant. The observer errors were proven to converge to the origin asymptotically. In the future, it is interesting to investigate globally asymptotically stable non-fragile observers for nonlinear systems with measurement noise.

DECLARATION OF COMPETING INTEREST

The authors declare that they do not have any commercial or associative interest that represents a conflict of interest in connection with the work submitted.

ACKNOWLEDGMENTS

This work was supported by National Natural Science Foundation of China (62273200), Hubei Key Laboratory of Hydroelectric Machinery Design and Maintenance (2021KJX04) and Yichang Key Laboratory of Defense and Control of Cyber-Physical Systems (2020XXRH01).

(Received August 22, 2023)

REFERENCES

- [1] U. Al-Saggaf, M. Bettayeb, and S. Djennoune: Fixed-time synchronization of memristor chaotic systems via a new extended high-gain observer. *European J. Control* *63* (2022), 1, 164–174. DOI:10.1016/j.ejcon.2021.10.002
- [2] C. Andreu and C. Ramon: Addressing the relative degree restriction in nonlinear adaptive observers: A high-gain observer approach. *J. Franklin Inst.* *359* (2022), 8, 3857–3882. DOI:10.1016/j.jfranklin.2022.03.020
- [3] D. Astolfi, L. Zaccarian, and M. Jungers: On the use of low-pass filters in high-gain observers. *Systems Control Lett.* *148* (2021), 104856. DOI:10.1016/j.sysconle.2020.104856
- [4] M. Chen and C. Chen: Robust nonlinear observer for Lipschitz nonlinear systems subject to disturbances. *IEEE Trans. Automat. Control* *52* (2007), 12, 2365–2369. DOI:10.1109/TAC.2007.910724
- [5] H. Chen and Y. Li: Stability and exact multiplicity of periodic solutions of Duffing equations with cubic nonlinearities. *Proc. Amer. Math. Soc.* *135* (2007), 12, 1–7.
- [6] C. Chen, C. Qian, Z. Sun, and Y. Liang: Global output feedback stabilization of a class of nonlinear systems with unknown measurement sensitivity. *IEEE Trans. Automat. Control* *63* (2018), 7, 2212–2217. DOI:10.1109/TAC.2017.2759274
- [7] W. Chen, H. Sun, and X. Lu: A variable gain impulsive observer for Lipschitz nonlinear systems with measurement noises. *J. Franklin inst.* *350* (2022), 18, 11186–11207.
- [8] D. Chowdhury, Y.K. Al-Nadawi, and X. Tan: Dynamic inversion-based hysteresis compensation using extended high-gain observer. *Automatica* *135* (2022), 109977. DOI:10.1016/j.automatica.2021.109977
- [9] G. Duan: High-order system approaches: III. observability and observer design. *ACTA Automat. Sinica* *46* (2020), 9, 1885–1895.

- [10] L. Dutta and D. Das: Nonlinear disturbance observer based multiple-model adaptive explicit model predictive control for nonlinear MIMO system. *Int. J. Robust Nonlinear Control* *33* (2023), 11, 5934–5955. DOI:10.1002/rnc.6680
- [11] X. Guo and G. Yang: Non-fragile H_∞ filter design for delta operator formulated systems with circular region pole constraints: an LMI optimization approach. *ACTA Automatica Sinica* *35* (2009), 9, 1209–1215. DOI:10.1016/S1874-1029(08)60106-8
- [12] C. Hua and X. Guan: Synchronization of chaotic systems based on PI observer design. *Physics Lett. A* *334* (2005), 5–6, 382–389. DOI:10.1016/j.physleta.2004.11.050
- [13] J. Huang and Z. Han: Adaptive non-fragile observer design for the uncertain Lur’e differential inclusion system. *Appl. Math. Modell.* *37* (2013), 1–2, 72–81.
- [14] C.S. Jeong, E.E. Yaz, and Y.I. Yaz: Resilient design of discrete-time observers with general criteria using LMIs. *Math. Computer Modell.* *42* (2005), 9–10, 931–938. DOI:10.1016/j.mcm.2005.06.004
- [15] H. Jian, H. Zhang, Y. Wang, and X. Liu: Adaptive state disturbance observer design for nonlinear system with unknown lipschitz constant. *Chinese Automation Congress 2015*, pp. 880–885.
- [16] M. Koo and H. Choi: State feedback regulation of high-order feedforward nonlinear systems with delays in the state and input under measurement sensitivity. *Int. J. Systems Sci.* *52* (2021), 10, 2034–2047. DOI:10.1080/00207721.2021.1876275
- [17] S. Lakshmanan and Y. Joo: Decentralized observer-based integral sliding mode control design of large-scale interconnected systems and its application to doubly fed induction generator-based wind farm model. *Int. J. Robust Nonlinear Control* *33* (2023), 10, 5758–5774. DOI:10.1002/rnc.6673
- [18] G. Li, D. Xu, and S. Zhou: A parameter-modulated method for chaotic digital communication based on state observers. *ATAC Physica Sinica* *53* (2004), 3, 706–709. DOI:10.1295/kobunshi.53.709
- [19] W. Li, X. Yao, and M. Krstic: Adaptive-gain observer-based stabilization of stochastic strict-feedback systems with sensor uncertainty. *Automatica* *120* (2020), 109112. DOI:10.1016/j.automatica.2020.109112
- [20] Z. Lin: Co-design of linear low-and-high gain feedback and high gain observer for suppression of effects of peaking on semi-global stabilization. *Automatica* *137* (2022), 110124. DOI:10.1016/j.automatica.2021.110124
- [21] L. Lin and Y. Shen: Adaptive anti-measurement-disturbance stabilization for a class of nonlinear systems via output feedback. *J. Control Theory Appl.* 2021. DOI:10.7641/CTA.2022.10773
- [22] Y. Liu and S. Fei: Chaos synchronization between the Sprott-B and Sprott-C with linear coupling. *ATAC Physica Sinica* *53* (2006), 3, 1035–1039.
- [23] C. Liu, K. Liao, K. Qian, Y. Li, and Q. Ding: The robust sliding mode observer design for nonlinear system with measurement noise and multiple faults. *Systems Engrg. Electron.* (2022).
- [24] R. Marino and P. Tomei: *Nonlinear Control Design: Geometric, Adaptive and Robust.* Prentice Hall, Hertfordshire 1995.
- [25] W. Perruquetti, T. Floquet, and E. Moulay: Finite-time observers: application to secure communication. *IEEE Trans. Automat. Control* *53* (2008), 1, 356–360. DOI:10.1109/TAC.2007.914264

- [26] Y. Shen, X. Xia: Semi-global finite-time observers for nonlinear systems. *Automatica* 44 (2008), 12, 3152–3156. DOI:10.1016/j.automatica.2008.05.015
- [27] F. E. Thau: Observing the state of nonlinear dynamic systems. *Int. J. Control* 17 (1973), 3, 471–479. DOI:10.1080/00207177308932395
- [28] Z. Xiang, R. Wang, and B. Jiang: Nonfragile observer for discrete-time switched nonlinear systems with time delay. *Circuits Systems Signal Process.* 30 (2011), 1, 73–87. DOI:10.1007/s00034-010-9210-8
- [29] G. Yang and J. Wang: Robust nonfragile kalman filtering for uncertain linear systems with estimator gain uncertainty. *IEEE Trans. Automat. Control* 46 (2001), 2, 343–348. DOI:10.1109/9.905707
- [30] Q. Zheng, S. Xu, and Z. Zhang: Nonfragile H-infinity observer design for uncertain nonlinear switched systems with quantization. *Appl. Math. Comput.* 386 (2020), 125435. DOI:10.1016/j.amc.2020.125435

*Fan Zhou, College of Electrical Engineering and New Energy, China Three Gorges University, Yichang, Hubei, 443002, P. R. China and State Grid Hubei Direct Current Operation Research Institute, Yichang, Hubei, 443000. P. R. China.
e-mail: 2944486543@qq.com*

*Yanjun Shen, Corresponding author. College of Electrical Engineering and New Energy, China Three Gorges University, Yichang, Hubei, 443002. P. R. China.
e-mail: shenyj@ctgu.cn*

*Zebin Wu, College of Electrical Engineering and New Energy, China Three Gorges University, Yichang, Hubei, 443002. P. R. China.
e-mail: 1142246293@qq.com*