

Monika Boschková

Self-tuning controls of linear stochastic systems in presence of drift

Kybernetika, Vol. 24 (1988), No. 5, 347--362

Persistent URL: <http://dml.cz/dmlcz/125623>

Terms of use:

© Institute of Information Theory and Automation AS CR, 1988

Institute of Mathematics of the Academy of Sciences of the Czech Republic provides access to digitized documents strictly for personal use. Each copy of any part of this document must contain these

Terms of use.



This paper has been digitized, optimized for electronic delivery and stamped with digital signature within the project *DML-CZ: The Czech Digital Mathematics Library*
<http://project.dml.cz>

SELF-TUNING CONTROLS OF LINEAR STOCHASTIC SYSTEMS IN PRESENCE OF DRIFT

MONIKA BOSCHKOVÁ

This paper deals with self-tuning controls constructed by inserting the estimates for the unknown parameters. The model of linear controlled system (5) containing a constant drift is considered. The unknown parameters are estimated by the least squares method. Recursive formula for the estimate is introduced and a sufficient condition for its consistency is presented. Assuming the consistency the asymptotic distributions of the estimate and of the quadratic functionals are investigated. From the asymptotic distributions the quality of the self-tuning can be assessed. At the end two examples are included for illustration.

1. INTRODUCTION

One of the methods for constructing self-tuning controls consists in expressing the calculated feedback gains as function of the unknown parameters and in substituting for the parameters their on-line estimates. This approach has been named the Principle of Estimation and Control. The monographs [4], [10] and the survey [3] contain the information of the present state of the subject. Generally speaking the approach can be identified with the Certainty Equivalence Principle. The latter is however mostly connected with the separation of the filtering and of the control in linear/quadratic control problems under indirect observation (see [2]) or with the Bayesian method.

The Estimation and Control Principle has been developed using the asymptotic theory of parameter estimation. The verification of the self-tuning property is of primary importance. Since the class of the self-tuning controls is usually extensive, it is advisable to apply additional criteria. By analogy with mathematical statistics asymptotic distribution of the parameter estimates or of certain cost functionals etc. are used to this purpose.

The subject of this paper are self-tuning controls of systems with constant drift. The paper continues the work done in [5], [6], [7]. When investigating controlled systems with known parameters the drift can be eliminated by transforming the

variables. Systems with unknown parameters require certain modifications of the basic methods. The modifications exhibit some additional properties of linear systems.

A typical example of the constant drift is the reference input r , function of which is to keep state vector near a prescribed quantity (see Fig. 1).

Let us present the following elementary model. The controlled system in Figure 2 is written in equations for the trajectories as

$$(1) \quad dX_t = -aX_t dt + dY_t + U_t dt,$$

$$(2) \quad dY_t = -bY_t dt + dW_t.$$

Inserting from the second equation into the first one we obtain

$$(3) \quad dX_t = -(aX_t + bY_t) dt + U_t dt + dW_t.$$

From (1) it follows

$$(4) \quad Y_t = X_t - X_0 - \int_0^t (-aX_s + U_s) ds + Y_0.$$

The integral in (4) is denoted by Z_t , hence,

$$dZ_t = (-aX_t + U_t) dt.$$

Substituting (4) for Y_t in (3) we get

$$dX_t = -(a + b)X_t dt - bZ_t dt + U_t dt + dW_t + c dt,$$

where

$$c = b(Y_0 - X_0).$$

In the case that only X_0 is observable, c is an unknown parameter and represents a constant drift.

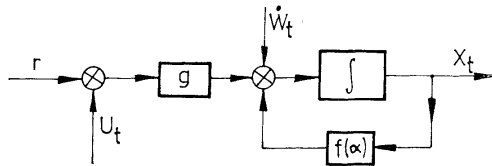


Fig. 1.

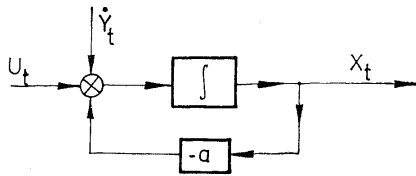


Fig. 2.

2. LEAST SQUARES METHOD

Let us consider the model of linear controlled system

$$(5) \quad dX_t = f(x) X_t dt + e(x) dt + gU_t dt + dW_t, \quad t \geq 0,$$

where

$$\alpha = (\alpha^0, \alpha^1, \dots, \alpha^q)'$$

is the $(q + 1)$ -dimensional vector of parameters,

$$\begin{aligned} f(x) &= f_0 + \alpha^0 f_1, \\ e(x) &= e_0 + \alpha^1 e_1 + \dots + \alpha^q e_q. \end{aligned}$$

Let the dimension of X_t and U_t be n and m , respectively. Let f_0, f_1 be $(n \times n)$ -matrices, e_0, e_1, \dots, e_q be n -dimensional vectors and let e_1, \dots, e_q be linearly independent. g is a constant matrix. $W = \{W_t, t \geq 0\}$ is the n -dimensional Wiener process with incremental variance matrix h , i.e.

$$E(W_t - W_s)(W_t - W_s)' = h(t - s), \quad t > s.$$

The parameter α is assumed to be unknown to the controller in this paper. The true value of α will be denoted by $\alpha_0 = (\alpha_0^0, \alpha_0^1, \dots, \alpha_0^q)$. The estimate α_T^* of α_0 from the observations of $X_t, t \in [0, T]$ is obtained by the least squares method.

To define α_T^* we introduce the discretized version of (5) and minimize the weighted sum of squares

$$(6) \quad \sum_k \frac{1}{\Delta t_k} (\Delta X_{t_k} - f(x) X_{t_k} \Delta t_k - e(x) \Delta t_k - gU_{t_k} \Delta t_k)'$$

$$l(\Delta X_{t_k} - f(x) X_{t_k} \Delta t_k - e(x) \Delta t_k - gU_{t_k} \Delta t_k),$$

where l is a positively semidefinite symmetric matrix. Equating the derivatives of (6) with respect to $\alpha^i, i = 0, \dots, q$, to zero we obtain the following relations

$$\begin{aligned} & \sum_k X_{t_k}' f_1' l f_1 X_{t_k} \Delta t_k \alpha^0 + \sum_{j=1}^q \sum_k X_{t_k}' f_1' l e_j \Delta t_k \alpha^j = \\ & = \sum_k X_{t_k}' f_1' l (\Delta X_{t_k} - f_0 X_{t_k} \Delta t_k - e_0 \Delta t_k - gU_{t_k} \Delta t_k), \\ & \sum_k e_i' l f_1 X_{t_k} \Delta t_k \alpha^0 + \sum_{j=1}^q \sum_k e_i' l e_j \Delta t_k \alpha^j = \\ & = \sum_k e_i' l (\Delta X_{t_k} - f_0 X_{t_k} \Delta t_k - e_0 \Delta t_k - gU_{t_k} \Delta t_k), \quad i = 1, \dots, q. \end{aligned}$$

From here we get letting $\Delta t_k \rightarrow 0$ the system of equations for α_T^*

$$(7) \quad \int_0^T X_t' f_1' l f_1 X_t dt \alpha_T^{0*} + \sum_{j=1}^q \int_0^T X_t' f_1' l e_j dt \alpha_T^{j*} =$$

$$= \int_0^T X_t' f_1' l (dX_t - f_0 X_t dt - e_0 dt - gU_t dt),$$

$$\int_0^T e_i' f_1 X_t dt \alpha_T^{0*} + \sum_{j=1}^q \int_0^T e_i' e_j dt \alpha_T^{j*} = \\ = \int_0^T e_i' l (dX_t - f_0 X_t dt - e_0 dt - g U_t dt), \quad i = 1, \dots, q.$$

The matrix of system (7) is denoted by A_T . It holds

$$(8) \quad A_T = \int_0^T Z_t' l Z_t dt,$$

where

$$Z_t = (f_1 X_t, e_1, \dots, e_q)'$$

From

$$dX_t - f_0 X_t dt - e_0 dt - g U_t dt = \alpha_0^0 f_1 X_t dt + \sum_{j=1}^q \alpha_0^j e_j dt + dW_t,$$

and from (7) it follows

$$(9) \quad A_T (\alpha_T^* - \alpha_0) = \int_0^T Z_t' l dW_t.$$

Next we demonstrate that α_t^* is a recursive estimate. Assume that the matrix A_t is nonsingular for $t \geq 0$. Set

$$P_t = (A_t)^{-1}.$$

From (8) it follows that

$$(10) \quad dP_t = -P_t Z_t' l Z_t P_t dt.$$

Using P_t the solution of equations (7) is expressed as

$$\alpha_T^* = P_T \int_0^T Z_t' l (dX_t - f_0 X_t dt - e_0 dt - g U_t dt).$$

Differentiating this equality and using (10) we get after rearrangements

$$(11) \quad d\alpha_t^* = P_t Z_t' l (dX_t - f(\alpha_t^*) X_t dt - e(\alpha_t^*) dt - g U_t dt).$$

The differential $d(\alpha_t^* - \alpha_0)$ is obtained by addition and subtraction of the term $f(\alpha_0) + e(\alpha_0)$ on the right-hand side of (11),

$$d(\alpha_t^* - \alpha_0) = P_t Z_t' l (dW_t - f(\alpha_t^* - \alpha_0) X_t dt - e(\alpha_t^* - \alpha_0) dt).$$

(5), (10), and (11) are differential equations for the trajectories of process X_t , the matrix P_t , and the estimate α_t^* .

Applying the recursive least squares estimation method (see [4]) to (6) and then letting $t_k \rightarrow 0$ we get the same result.

3. THE SELF-TUNING PROPERTY

Next we investigate the consistency of the estimate α_t^* . We recall equation (5) and assume that a design method, which yields the control U_t in the feedback form

$$U_t = k(\alpha) X_t + k_0(\alpha),$$

has been selected. The pole assignment method or optimal stationary controls with respect to quadratic cost can be mentioned as examples.

Since the true value α_0 is unknown, α_0 is replaced by the least squares estimate

α_t^* . This leads to

$$(12) \quad U_t = k(\alpha_t^*) X_t + k_0(\alpha_t^*) = k_t^* X_t + k_{0t}^* .$$

The sets $\mathcal{K} = \{k(\alpha), \alpha \in \mathbb{R}^{q+1}\}$, $\mathcal{K}_0 = \{k_0(\alpha), \alpha \in \mathbb{R}^{q+1}\}$ are supposed to be bounded. This can be usually achieved by slightly modifying the design method. To guarantee the stability of the system under control (12) we make a global Liapunov type hypothesis.

Assumption I. There exists a positively definite matrix z such that the matrices

$$z(f + gk) + (f + gk)'z + I, \quad k \in \mathcal{K},$$

are negatively semidefinite.

Further some consequences of this assumption are derived.

Considering any nonanticipative control in the form

$$U_t = K_t X_t + K_{0t}, \quad K_t \in \mathcal{K}, \quad K_{0t} \in \mathcal{K}_0,$$

the equation (5) is rewritten as

$$dX_t = (f + gK_t) X_t dt + (e + gK_{0t}) dt + dW_t .$$

Let $X_0 = x$. From the Itô formula it follows

$$(13) \quad X_T' z X_T - x' z x = 2 \int_0^T X_t' z (f + gK_t) X_t dt + 2 \int_0^T X_t' z (e + gK_{0t}) dt + 2 \int_0^T X_t' z dW_t + T \operatorname{tr}(zh) .$$

Assumption I implies that the first term on the right-hand side of (13) is smaller than

$$- \int_0^T |X_t|^2 dt .$$

Since $|z(e + gK_{0t})|$ is bounded by a constant z_0 , we have

$$(14) \quad \mathbb{E} X_T' z X_T + \mathbb{E} \int_0^T |X_t|^2 dt - 2z_0 \int_0^T |X_t| dt \leq T \operatorname{tr}(zh) + x' z x .$$

By the Schwarz inequality it follows from (14)

$$\mathbb{E} \frac{1}{T} \int_0^T |X_t|^2 dt - 2z_0 \left(\frac{1}{T} \int_0^T |X_t| dt \right)^{1/2} \leq \operatorname{tr}(zh) + o_p(1) .$$

Hence,

$$(15) \quad \mathbb{E} \frac{1}{T} \int_0^T |X_t|^2 dt \leq C_0 ,$$

where

$$(16) \quad C_0 = (z_0^2 + \sqrt{(z_0^2 + \operatorname{tr} zh)})^2$$

independently of the control and the initial state.

Analogously from (13) we obtain

$$\frac{1}{T} \left(X_T' z X_T + \int_0^T |X_t|^2 dt - 2z_0 \int_0^T |X_t| dt \right) \leq \operatorname{tr}(zh) + \frac{1}{T} \left(x' z x + 2 \int_0^T X_t' z dW_t \right) .$$

(15) implies that the last term on the right-hand side converges to zero a.s. Letting $T \rightarrow \infty$ we get

$$(17) \quad \overline{\lim}_{T \rightarrow \infty} \frac{1}{T} \int_0^T |X_t|^2 dt \leq C_0.$$

Similar reasoning applied to $(X'_T z X_T)^2$ yields

$$(18) \quad \lim_{T \rightarrow \infty} |X_T|^2/T = 0 \quad \text{a.s.}$$

The relations (17) and (18) are used in the proof of the following proposition.

Proposition 1. Let Assumption 1 holds, let $\sqrt{(l)} e_i$, $i = 1, \dots, q$, be linearly independent. If $f_1 \neq 0$ (i.e. the parameter α_0 is not absent), let $\sqrt{(l)} f_1 \sqrt{(h)} \neq 0$. Then, as $t \rightarrow \infty$,

$$\alpha_t^* \rightarrow \alpha_0 \quad \text{a.s.}$$

Proof. Equation (9) is multiplied from left by $(\alpha_T^* - \alpha_0)'/T$. This yields

$$(19) \quad (\alpha_T^* - \alpha_0)' \frac{1}{T} \int_0^T Z_t' l Z_t dt (\alpha_T^* - \alpha_0) = (\alpha_T^* - \alpha_0)' \frac{1}{T} \int_0^T Z_t' l dW_t.$$

Denote for $\mu = (\mu^0, \dots, \mu^q)'$

$$L_T(\mu) = \mu' \frac{1}{T} \int_0^T Z_t' l Z_t dt \mu.$$

$L_T(\mu)/T$ is a quadratic-linear functional of the trajectory of the form

$$L_T(\mu) = \frac{1}{T} \int_0^T (X_t' q(\mu) X_t + X_t' q_0(\mu)) dt + q_1(\mu),$$

where

$$(20) \quad \begin{aligned} q(\mu) &= (\mu^0)^2 f_1' l f_1, \\ q_0(\mu) &= 2\mu^0 f_1' \sqrt{(l)} (\sqrt{(l)} \sum_{j=1}^q e_j \mu^j), \\ q_1(\mu) &= (\sqrt{(l)} \sum_{j=1}^q e_j \mu^j)' (\sqrt{(l)} \sum_{j=1}^q e_j \mu^j). \end{aligned}$$

If $f_1 = 0$, then $L_T(\mu) = q_1(\mu)$, (34) holds and the proof of the proposition is simple. Let $f_1 \neq 0$. The equation of the system can be considered in the form

$$dX_t = f(\alpha_0) X_t dt + e(\alpha_0) dt + g U_t dt + dW_t = S_t dt + dW_t.$$

Set for fixed μ

$$Q_T(\mu) = \int_0^T (X_t' q(\mu) X_t + X_t' q_0(\mu)) dt + c \int_0^T |S_t|^2 dt.$$

We shall deal with the problem of minimizing the average cost $Q_T(\mu)/T$, as $T \rightarrow \infty$. The minimum is denoted by $\Theta_c(\mu)$. To obtain $\Theta_c(\mu)$ we solve the stationary Bellman equation

$$(21) \quad \inf_s [\nabla V(y) s + \frac{1}{2} \text{tr} (h \nabla' \nabla V(y)) + y' q y + y' q_0 + c |s|^2 - \Theta_c] = 0,$$

tr denotes the trace operator. The solution of this equation is found in the form

$$(22) \quad V(y) = y'v_y + y'v_0.$$

Inserting (22) into (21) we get

$$(23) \quad \inf_s [(2y'v + v_0')s + \text{tr}(hv) + y'q_y + y'q_0 + cs's - \Theta_c] = 0.$$

By differentiating the term in the square brackets with respect to s we obtain the optimal value of s

$$s = -(2v_y + v_0)/2c,$$

which is substituted into (23) again. This yields the following equations for v , v_0 , and $\Theta_c(\mu)$,

$$(24) \quad -v^2/c + q = 0,$$

$$(25) \quad v_0'v/c + q_0' = 0,$$

$$(26) \quad -v_0'v_0/4c + \text{tr}(hv) - \Theta_c = 0.$$

From (24) and (20) it follows that

$$v = \sqrt{(c)} |\mu^0| (f_1' f_1)^{1/2}.$$

The symmetric matrix $f_1' f_1$ can be expressed as

$$f_1' f_1 = Y \begin{bmatrix} \lambda_1 & & & & \\ & \ddots & & & \\ & & \lambda_p & & \\ & & & 0 & \\ & & & & \ddots \\ & & & & & 0 \end{bmatrix} Y' = Y \Lambda Y',$$

where Y is an orthogonal matrix built from the characteristic vectors. It holds that

$$(f_1' f_1)^{1/2} = Y \begin{bmatrix} \sqrt{\lambda_1} & & & & \\ & \ddots & & & \\ & & \sqrt{\lambda_p} & & \\ & & & 0 & \\ & & & & \ddots \\ & & & & & 0 \end{bmatrix} Y'.$$

First suppose that $f_1' f_1$ is nonsingular, i.e. $p = n$. Then from (25)

$$v_0 = \pm 2 \sqrt{(c)} (f_1' f_1)^{-1/2} f_1' \sqrt{(l)} (\sqrt{(l)} \sum_{j=1}^q e_j \mu^j).$$

Hence,

$$v_0' v_0 / (4c) = (\sqrt{(l)} \sum_{j=1}^q e_j \mu^j)' \sqrt{(l)} f_1 (f_1' f_1)^{-1} f_1' \sqrt{(l)} \cdot (\sqrt{(l)} \sum_{j=1}^q e_j \mu^j) = q_1(\mu).$$

Let $f_1' f_1$ be singular. To prove the solvability of (25) multiply v_0 from the left

by the i th column of Y ,

$$y^i v v_0 = \sqrt{(c)} |\mu^0| \sqrt{(\lambda_i)} y^i v_0.$$

From (25) and (20) it follows

$$(27) \quad \sqrt{(c)} |\mu^0| \sqrt{(\lambda_i)} y^i v_0 = -2\mu^0 c b_i,$$

where

$$b_i = y^i f'_1 \sqrt{(l)} \left(\sqrt{(l)} \sum_{j=1}^q e_j \mu^j \right).$$

If $\lambda_i = 0$, then $b_i = 0$. Hence,

$$v_0 = \pm \sum_{i=1}^p 2 \sqrt{(c)} \frac{1}{\lambda_i} b_i y^i$$

is a solution of (25) and

$$v'_0 v_0 / (4c) = \sum_{i=1}^p \frac{b_i^2}{\lambda_i}.$$

Limit passage using nonsingular matrices enables us to deduce from (27) the inequality

$$v'_0 v_0 / (4c) \leq q_1(\mu).$$

Finally from (26) it follows that

$$(28) \quad \Theta_c(\mu) + q_1(\mu) \geq \text{tr}(h v) = \sqrt{(c)} |\mu^0| \text{tr}(h(f'_1 l f_1)^{1/2}).$$

Since $\sqrt{(l)} f'_1 \sqrt{(h)} \neq 0$, the following matrices are nonzero

$$\sqrt{(h)} (f'_1 l f_1) \sqrt{(h)}, \quad \sqrt{(h)} (f'_1 l f_1)^{1/4}, \quad \sqrt{(h)} (f'_1 l f_1)^{1/2} \sqrt{(h)}.$$

The trace of the last matrix equals $\text{tr}(h(f'_1 l f_1)^{1/2})$, which consequently is positive.

Denote by $\varphi(y, s)$ the term in the square brackets in (21). According to (21) $\varphi(y, s) \geq 0$ for $s \in \mathbb{R}^n$. The Itô formula gives

$$\int_0^T dV(X_t) = \int_0^T \varphi(X_t, S_t) dt + \int_0^T \nabla V(X_t) dW_t - Q_T + \Theta_c T.$$

Hence,

$$(29) \quad \frac{1}{T} Q_T - \Theta_c \geq \frac{1}{T} (V(X_0) - V(X_T) + \int_0^T \nabla V(X_t) dW_t).$$

The right-hand side of (29) converges to zero a.s. in virtue of (17) and (18). It results

$$(30) \quad \varliminf_{T \rightarrow \infty} Q_T / T \geq \Theta_c.$$

It follows from (30) that

$$\varliminf_{T \rightarrow \infty} L_T(\mu) \geq \Theta_c(\mu) + q_1(\mu) - c \overline{\lim}_{T \rightarrow \infty} \frac{1}{T} \int_0^T |S_t|^2 dt.$$

Since (17) holds,

$$\overline{\lim}_{T \rightarrow \infty} \frac{1}{T} \int_0^T |S_t|^2 dt \leq C_1$$

for some constant C_1 . Hence,

$$(31) \quad \varliminf_{T \rightarrow \infty} L_T(\mu) \geq \Theta_c(\mu) + q_1(\mu) - c C_1.$$

We aim to fulfil

$$(32) \quad \lim_{T \rightarrow \infty} L_T(\mu) \geq \delta, \quad \mu \in \mathbb{R}^{q+1}, \quad |\mu| = 1, \quad \text{a.s.},$$

for a $\delta > 0$.

If $|\mu^0| = 0$, then $q(\mu) = q_0(\mu) = 0$ and

$$L_T(\mu) = q_1(\mu) \geq \delta_1, \quad |\mu| = 1, \quad \text{with } \delta_1 > 0$$

as follows from (20) and from the assumption that $\sqrt{(l)} e_i, i = 1, \dots, q$, are linearly independent. Relation (17) implies the uniform continuity of $L_T(\mu)$ in $\mu, |\mu| = 1$. This gives the validity of $L_T(\mu) \geq \frac{1}{2}\delta_1, T > 0$, for $\mu, |\mu| = 1$, with $|\mu^0|$ sufficiently small, i.e. $|\mu^0| \leq \gamma, \gamma > 0$. From (31) and (28)

$$(33) \quad \lim_{T \rightarrow \infty} L_T(\mu) \geq \sqrt{(c)} |\mu^0| \text{tr}(h(f'_1 l f_1)^{1/2}) - cC_1.$$

For $|\mu^0| > \gamma$ there exists $c > 0$ such that the right-hand side of (33) is positive. Using the uniform continuity of $L_T(\mu)$ in $\mu, |\mu| = 1$, we get (32). Hence,

$$(34) \quad \lim_{T \rightarrow \infty} (\alpha_T^* - \alpha_0) \frac{1}{T} \int_0^T Z'_t l Z_t dt (\alpha_T^* - \alpha_0) \geq \delta |\alpha_T^* - \alpha_0|^2 \text{ a.s.}$$

From (19) it follows

$$\lim_{T \rightarrow \infty} \left| \frac{1}{T} \int_0^T Z'_t l dW_t \right| \geq \delta |\alpha_T^* - \alpha_0|.$$

On the other hand

$$\frac{1}{T} \int_0^T Z'_t l dW_t$$

converges to zero a.s., as $T \rightarrow \infty$, provided (17) holds, as it is seen by expressing the integral by means of a random time change in a Wiener process. Hence,

$$\alpha_t^* \rightarrow \alpha_0 \quad \text{a.s., } t \rightarrow \infty,$$

is a consequence of (34). □

4. ASYMPTOTIC RESULTS

In this section the limit distribution of the estimate and of quadratic functionals will be derived.

Assume first that the true value α_0 is known and consider the control in the form

$$(35) \quad U_t = k(\alpha_0) X_t + k_0(\alpha_0) = kX_t + k_0.$$

Then (5) becomes

$$(36) \quad dX_t = (f + gk) X_t dt + (e + gk_0) dt + dW_t.$$

Provided that the matrix $f + gk$ is stable, X_t has as $t \rightarrow \infty$ asymptotically normal

distribution $N(m, v)$, where m and v fulfil the following equations

$$(37) \quad (f + gk)m + (e + gk_0) = 0,$$

$$(38) \quad (f + gk)v + v(f + gk)' + h = 0.$$

Set

$$\bar{X}_t = X_t - m.$$

From (36) it follows

$$(39) \quad d\bar{X}_t = (f + gk)\bar{X}_t dt + dW_t.$$

In the case that the true value α_0 is unknown, (12) is used, i.e.

$$(40) \quad U_t = k(\alpha_t^*)X_t + k_0(\alpha_t^*) = k_t^*X_t + k_{0t}^*.$$

(5) can be then rewritten as

$$(41) \quad d\bar{X}_t = (f + gk_t)\bar{X}_t dt + g((k_t^* - k)m + (k_{0t}^* - k_0)) dt + dW_t.$$

Note that (39) is the limit case of (41) for $k_t^* \rightarrow k$ and $k_{0t}^* \rightarrow k_0$ as $t \rightarrow \infty$.

Next we shall study the asymptotic behaviour of quadratic cost

$$(42) \quad C_T = \int_0^T (\bar{X}_t' c \bar{X}_t + \bar{X}_t' c_0) dt$$

as $T \rightarrow \infty$. When X_t is used instead of \bar{X}_t , the cost can be transformed to the form (42) up to an additive constant. The mean of the integrand in (42) with respect to the limit distribution $N(0, v)$ is

$$E_\infty(\bar{X}_t' c \bar{X}_t + \bar{X}_t' c_0) = \text{tr}(vc).$$

Denote by $\Theta = \text{tr}(vc)$ the limiting average cost.

The cost potential for initial state $X_0 = x$ and control (35) has the expression

$$P_x = \int_0^\infty E_x(\bar{X}_t' c \bar{X}_t + \bar{X}_t' c_0) dt.$$

It can be proved that

$$P_x = \bar{x}' w \bar{x} + \bar{x}' w_0 + \text{const.},$$

where $\bar{x} = x - m$, and w and w_0 fulfil the equations

$$(43) \quad w(f + gk) + (f + gk)' w + c = 0,$$

$$(44) \quad (f + gk)' w_0 + c_0 = 0.$$

We shall need the following equation for investigating the asymptotic behaviour of C_T as $T \rightarrow \infty$.

Lemma 1. For any nonanticipative control of the form $U_t = K_t X_t + K_{0t}$ it holds

$$(45) \quad \begin{aligned} C_T - T\Theta + \bar{X}_T' w \bar{X}_T + \bar{X}_T' w_0 - \bar{x}' w \bar{x} - \bar{x}' w_0 - \\ - \int_0^T (2w\bar{X}_t + w_0)' g((K_t - k)\bar{X}_t + (K_t - k)m + (K_{0t} - k_0)) dt = \\ = \int_0^T (2w\bar{X}_t + w_0)' dW_t. \end{aligned}$$

Proof. Using the Itô formula and the relation (41) for $U_t = K_t X_t + K_{0t}$, we get

$$\begin{aligned} \bar{X}'_T w \bar{X}_T - \bar{x}' w \bar{x} &= \int_0^T d\bar{X}'_t w \bar{X}_t = \\ &= 2 \int_0^T \bar{X}'_t w ((f + gK_t) \bar{X}_t + g(K_t - k) m + g(K_{0t} - k_0)) dt + \\ &\quad + 2 \int_0^T \bar{X}'_t w dW_t + T \operatorname{tr}(wh). \end{aligned}$$

Analogously

$$\begin{aligned} \bar{X}'_T w_0 - \bar{x}' w_0 &= w'_0 \int_0^T d\bar{X}_t = \\ &= w'_0 \int_0^T ((f + gK_t) \bar{X}_t + g(K_t - k) m + g(K_{0t} - k_0)) dt + w'_0 \int_0^T dW_t. \end{aligned}$$

Further, it holds

$$\operatorname{tr}(wh) = \operatorname{tr}(vc) = \Theta.$$

To obtain this result equation (38) is multiplied from left by the matrix w and equation (43) from right by the matrix v and the trace operator is applied to both equations. Hence,

$$\begin{aligned} (46) \quad C_T - T\Theta + \bar{X}'_T w \bar{X}_T + \bar{X}'_T w_0 - \bar{x}' w \bar{x} - \bar{x}' w_0 &= \\ &= \int_0^T (\bar{X}' c \bar{X} + \bar{X}' c_0) dt + \int_0^T (2\bar{X}' w + w'_0) dW + \\ &+ \int_0^T (2\bar{X}' w + w'_0) ((f + gK) \bar{X} + g(K - k) m + g(K_0 - k_0)) dt = \\ &= \int_0^T (\bar{X}' c \bar{X} + 2\bar{X}' w (f + gk) \bar{X}) dt + \int_0^T (\bar{X}' c_0 + w'_0 (f + gk) \bar{X}) dt + \\ &+ \int_0^T (2\bar{X}' w + w'_0) g((K - k) \bar{X} + (K - k) m + (K_0 - k_0)) dt + \\ &\quad + \int_0^T (2\bar{X}' w + w'_0) dW. \end{aligned}$$

The first two integrals on the right-hand side of (46) are equal to zero in consequence of relations (43) and (44). This implies the validity of (45). \square

Next we return to the system of equations (7) for the estimate α_t^* . Assume the strong consistency of α_t^* , i.e.

$$(47) \quad \alpha_t^* \rightarrow \alpha_0 \quad \text{a.s. as } t \rightarrow \infty,$$

and make the following hypothesis.

Assumption 2. The matrix $f + gk$ is stable, and $k(x)$ and $k_0(x)$ are continuous at α_0 .

Since the Liapunov condition is fulfilled in a neighbourhood of α_0 , the results from previous section can be used in the proof that the law of large numbers holds for quadratic functionals (see [2]). Hence, by the law of large numbers A_T/T converges as $T \rightarrow \infty$ to the matrix $a = (a_{ij})_{i,j=0,\dots,q}$ fulfilling

$$\begin{aligned} a_{00} &= \operatorname{tr}(f'_1 l f_1 v) + m' f'_1 l f_1 m, \\ a_{0i} &= a_{i0} = m' f'_1 l e_i, \quad i = 1, \dots, q, \\ a_{ij} &= a_{ji} = e'_i l e_j, \quad i, j = 1, \dots, q. \end{aligned}$$

The matrix a is supposed to be nonsingular. Then, according to (9),

$$(48) \quad (\alpha_T^* - \alpha_0) \sim a^{-1} \frac{1}{T} \int_0^T Z_t' l dW_t.$$

Denote for $z \in [0, 1]$

$$\begin{aligned} {}^z Y_T &= ({}^z Y_T^0, {}^z Y_T^1, \dots, {}^z Y_T^q, {}^z Y_T^{q+1})' = \\ &= \frac{1}{\sqrt{T}} (\int_0^{Tz} X_t' f_1' l dW_t, \int_0^{Tz} e_1' l dW_t, \dots, \int_0^{Tz} e_q' l dW_t, \int_0^{Tz} (2w\bar{X}_t + w_0)' dW_t)'. \end{aligned}$$

We shall study the limit distribution of the process $\{{}^z Y_T, z \in [0, 1]\}$ as $T \rightarrow \infty$. Consider, e.g. the element

$$(49) \quad {}^z Y_T^0 = \frac{1}{\sqrt{T}} \int_0^{Tz} X_t' f_1' l dW_t = \frac{1}{\sqrt{T}} \mathcal{W}_{T(v\tau_z)T} = {}^T \mathcal{W}_{V_{Tz}l/T},$$

where ${}^T \mathcal{W}_u$ is a Wiener process and

$$V_{Tz} = \int_0^{Tz} X_t' f_1' l h l f_1 X_t dt$$

by the known representation of Wiener integrals.

V_T/T approaches as $T \rightarrow \infty$ the value

$$b = \text{tr}(f_1' l h l f_1 v) + m' f_1' l h l f_1 m$$

according to the law of large numbers. This consideration indicates that the process $\{{}^z Y_T^0, z \in [0, 1]\}$ converges weakly as $T \rightarrow \infty$ to the Wiener process fulfilling $(dZ)^2 = b dt$. When we investigate all the vector ${}^z Y_T, z \in [0, 1]$, we take linear combination of its elements and prove using the same consideration that the process $\{{}^z Y_T, z \in [0, 1]\}$ converges weakly as $T \rightarrow \infty$ to the $(q+2)$ -dimensional Wiener process

$$(50) \quad (\mathcal{W}_z^0, \mathcal{W}_z^1, \dots, \mathcal{W}_z^q, \mathcal{W}_z^{q+1})' = (\tilde{\mathcal{W}}_z^0, \mathcal{W}_z^{q+1})', z \in [0, 1],$$

with incremental variance matrix

$$\begin{pmatrix} b & p \\ p & d \end{pmatrix},$$

where

$$d = 4 \text{tr}(whw'v) + w_0' h w,$$

p is the $(1+q)$ -dimensional vector with elements

$$p_0 = 2 \text{tr}(v f_1' l h w) + m' f_1' l h w_0,$$

$$p_i = e_i' l h w_0, \quad i = 1, \dots, q,$$

and b is the $((1+q) \times (1+q))$ -matrix, the elements of which are

$$b_{00} = \text{tr}(f_1' l h l f_1 v) + m' f_1' l h l f_1 m,$$

$$b_{0i} = b_{i0} = m' f_1' l h l e_i, \quad i = 1, \dots, q,$$

$$b_{ij} = b_{ji} = e_i' l h l e_j, \quad i, j = 1, \dots, q.$$

Using this limit relation for ${}^z Y_T$ and using (48) we get the following proposition.

Proposition 2. Let Assumption 2 and (47) hold, and let the matrix a be nonsingular. Then $\sqrt{(T)}(z_T^* - z_0)$ has asymptotic distribution $N(0, a^{-1}ba^{-1})$ as $T \rightarrow \infty$.

Next the equation (45) is used for C_{Tz} , i.e.

$$C_{Tz} - \Theta Tz = \int_0^z (2w\bar{X}_t + w_0)' g((k_t^* - k)\bar{X}_t + (k_t^* - k)m + (k_0^* - k_0)) dt + \int_0^z (2w\bar{X}_t + w_0)' dW_t + o_p(\sqrt{T}).$$

The integrand of the first integral on the right-hand side is denoted by I_1 . Provided that the functions $k(z)$, $k_0(z)$ are twice continuously differentiable at z_0 , we can use their Taylor development at z_0 . Set

$$\frac{\partial}{\partial z^i} k(z_0) = k^i, \quad \frac{\partial}{\partial z^i} k_0(z_0) = k_0^i, \quad i = 0, \dots, q,$$

and

$$(51) \quad u_i(\bar{X}) = (2w\bar{X} + w_0)' g(k^i\bar{X} + k^i m + k_0^i), \quad i = 0, \dots, q.$$

Then

$$I_1 = \sum_{i=0}^q u_i(\bar{X}_t) (z_t^{i*} - z_0^i) + o_p(|\bar{X}_t|^2 + 1) |z_t^{i*} - z_0^i|^2,$$

and hence,

$$C_{Tz} - \Theta Tz = \sum_{i=0}^q \int_0^z \frac{1}{t} \int_0^t u_i(\bar{X}_s) ds (z_t^{i*} - z_0^i) dt + \sqrt{(T)} {}^z Y_T^{q+1} + o_p(\sqrt{T}).$$

Using the substitution $t = yT$ we get after rearrangements

$$C_{Tz} - \Theta Tz = \sum_{i=0}^q \int_0^z \frac{1}{y} \int_0^{yT} u_i(\bar{X}_s) ds (z_{yT}^{i*} - z_0^i) dy + \sqrt{(T)} {}^z Y_T^{q+1} + o_p(\sqrt{T}).$$

From (48) it follows

$$\sqrt{(T)}(z_{Tz}^{*i} - z_0^i) \sim j_i a^{-1} \frac{1}{z} {}^z \tilde{Y}_T,$$

where ${}^z \tilde{Y}_T = ({}^z Y_T^0, \dots, {}^z Y_T^q)'$ and j_i is the row vector having 1 at i th position and 0 elsewhere. Hence,

$$\begin{aligned} \frac{1}{\sqrt{T}}(C_{Tz} - \Theta Tz) &= \sum_{i=0}^q \int_0^z \frac{1}{Tt} \int_0^{tT} u_i(\bar{X}_s) ds \sqrt{(T)}(z_{tT}^{i*} - z_0^i) dt + {}^z Y_T^{q+1} + o_p(1) = \\ &= \sum_{i=0}^q \int_0^z \frac{1}{Tt} \int_0^{tT} u_i(\bar{X}_s) ds \frac{1}{t} j_i a^{-1} {}^z \tilde{Y}_T dt + {}^z Y_T^{q+1} + o_p(1). \end{aligned}$$

From (51) applying the law of large numbers it can be established that

$$\frac{1}{T} \int_0^T u_i(\bar{X}_s) ds, \quad i = 0, \dots, q,$$

approaches as $T \rightarrow \infty$ the value

$$r^i = 2 \operatorname{tr}(wgk^i v) + w_0' g k^i m + w_0' g k_0^i, \quad i = 0, \dots, q.$$

This yields using (49) and (50) that $(C_{Tz} - \Theta Tz)/\sqrt{T}$ converges weakly as $T \rightarrow \infty$ to

$$\int_0^z \frac{1}{t} \sum_{i=0}^q r^i j_i a^{-1} \tilde{W}_t dt + \mathcal{W}_z^{q+1}.$$

Set $r = (r^0, r^1, \dots, r^q)'$. From the above consideration the following proposition can be formulated.

Proposition 3. Let the matrix a be nonsingular and let the functions $k(\alpha)$, $k_0(\alpha)$ be twice continuously differentiable at α_0 . Assume

$$U_t = k(\alpha_t^*) X_t + k_0(\alpha_t^*), \quad t \geq 0,$$

where α_t^* is the least squares estimate of α_0 satisfying

$$\lim_{t \rightarrow \infty} \alpha_t^* = \alpha_0 \quad \text{a.s.}$$

Then the distribution of the process $\{(C_{Tz} - \Theta Tz)/\sqrt{T}, z \in [0, 1]\}$ converges weakly as $T \rightarrow \infty$ to the distribution of

$$\int_0^z \frac{1}{t} Z_t^1 dt + Z_z^2, \quad z \in [0, 1],$$

where $Z = \{(Z_t^1, Z_t^2), t \in [0, 1]\}$ is the two-dimensional Wiener process with incremental variance matrix

$$\begin{pmatrix} r' a^{-1} b a^{-1} r & p' a^{-1} r \\ p' a^{-1} r & d \end{pmatrix}.$$

5. EXAMPLES

5.1. Elimination of the drift

We shall consider the model of linear controlled system

$$dX_t = fX_t dt + e(\alpha) dt + U_t dt + dW_t, \quad t \geq 0,$$

where

$$e(\alpha) = e_0 + e_1 \alpha^1 + \dots + e_q \alpha^q.$$

Assume that α_0 , the true value of parameter $\alpha = (\alpha^1, \dots, \alpha^q)'$, is unknown. The least squares estimate α_t^* satisfies the following system of equations

$$(52) \quad \sum_{j=1}^q \int_0^T e_j' e_j dt \alpha_t^{j*} = \int_0^T e_j' (dX_t - fX_t dt - e_0 dt - U_t dt), \quad i = 1, \dots, q.$$

Denote by a a $(q \times q)$ -matrix with elements

$$a_{ij} = e_j' e_j, \quad i, j = 1, \dots, q,$$

and suppose that a is nonsingular. From (52) we obtain

$$(53) \quad \sqrt{(T)}(\alpha_T^* - \alpha_0) = a^{-1}(e_1, \dots, e_q)' \sqrt{W_T} / \sqrt{(T)} = a^{-1} e' \sqrt{W_T} / \sqrt{(T)}.$$

Since W_T/\sqrt{T} has distribution $N(0, h)$, it holds

$$\sqrt{T}(\alpha_T^* - \alpha_0) \sim N(0, a^{-1}e'lhlea^{-1}).$$

To offset the drift $e(x)$ we introduce the control in the form $U_t = -e(\alpha_t^*)$. Hence,

$$dX_t = fX_t dt + e(\alpha_0) dt - e(\alpha_t^*) dt + dW_t.$$

Using the matrix $F(t) = \exp(tf)$ and the relation (53) for $(\alpha_t^* - \alpha_0)$ the expression for X_t is obtained in the form

$$X_t = F(t)(X_0 + \int_0^t F(s)^{-1}(f + bs^{-1})W_s ds) + W_t,$$

where

$$b = -ea^{-1}e'l.$$

Computation of the variance matrix

$$q(t) = E(X_t - EX_t)(X_t - EX_t)'$$

yields

$$q(t) = \tilde{q}(t) - q_1/t + o(t^{\delta-2}), \quad t \rightarrow \infty, \quad \delta > 0,$$

where $\tilde{q}(t)$ denotes the variance matrix of \tilde{X}_t fulfilling

$$d\tilde{X}_t = f\tilde{X}_t dt + dW_t,$$

and q_1 satisfies the equation

$$fq_1 + q_1f' + (bhb' + bh)f^{-1} + f^{-1}(bhb' + bh)' = 0.$$

5.2. Recursive model of self-tuning control

Let

$$(54) \quad dX_t = \alpha fX_t dt + gU_t dt + dW_t,$$

where U_t is one-dimensional. We look for k such that for $U_t = -k'X_t$ the system (54) has a transfer function with beforehand selected poles, i.e.

$$0 = \det(zI - \alpha f + gk') = D(z) = z^n + d_1 z^{n-1} + \dots + d_{n-1}z + d_n,$$

where d_1, \dots, d_n are fixed.

According to the Ackermann formula (see [1]) this k has the following expression

$$k' = (0, \dots, 0, 1)(g, \alpha fg, \alpha^2 f^2 g, \dots, \alpha^{n-1} f^{n-1} g)^{-1} D(\alpha f).$$

After rearrangements we get

$$(55) \quad k' = (0, \dots, 0, 1)(g, fg, f^2 g, \dots, f^{n-1} g)^{-1} \cdot (f^n \alpha + d_1 f^{n-1} + \sum_{i=1}^{n-1} d_{i+1} f^{n-1-i} \alpha^{-i}).$$

In the case that the parameter α is unknown, we use the least squares estimate α_t^* fulfilling the recursive relations

$$\begin{aligned} d\alpha_t^* &= P_t X_t' f' l (dX_t - \alpha_t^* f X_t - g k_t' X_t dt), \\ dP &= -P_t^2 X_t' f' l f X_t dt, \end{aligned}$$

as follows from (11). Applying the Itô formula to $d(\alpha_t^*)^i$ we obtain from (55) the recursive expression for the estimate of the control k

$$dk_t = (0, \dots, 0, 1) (g, fg, \dots, f^{n-1}g)^{-1} \cdot [f^n d\alpha_t^* + \sum_{i=1}^{n-1} d_{i+1} f^{n-i-1} (i(\alpha_t^*)^{-i-1} d\alpha_t^* + \frac{1}{2}i(i+1)(\alpha_t^*)^{-i-2} (d\alpha_t^*)^2)].$$

(Received January 29, 1988.)

REFERENCES

- [1] J. Ackerman: Der Entwurf linearer Regelungssysteme im Zustandsraum. Regelungstechnik u. Prozess-Datenverarb. 20 (1972), 297–300.
- [2] K. J. Åström: Introduction to Stochastic Control Theory. J. Wiley, New York 1970.
- [3] P. R. Kumar: A survey of some results in stochastic adaptive control. SIAM J. Control Optim. 23 (1985), 329–380.
- [4] P. R. Kumar and P. Varaiya: Stochastic Systems: Estimation, Identification, and Adaptive Control. Prentice Hall, Engelwood Cliffs 1986.
- [5] P. Mandl: Some connections between statistics and control theory. In: Mathematical Statistics and Probability, Vol. B. D. Reidel, Dordrecht 1987, 155–168.
- [6] P. Mandl: On evaluating the performance of self-tuning regulators. In: Proc. 2nd International Symp. on Numerical Analysis, Prague 1987. B. G. Teubner, Leipzig. To appear.
- [7] P. Mandl, T. E. Duncan and B. Pasik-Duncan: On the consistency of a least squares identification. Kybernetika 24 (1988), 5, 340–346.
- [8] J. M. Mendel: Discrete Techniques of Parameter Estimation. Marcel Dekker, New York 1973.
- [9] M. B. Nevelson and R. Z. Khasminsky: Stochastic Approximation and Recursive Estimation (in Russian). Nauka, Moscow 1972.
- [10] B. Pasik-Duncan: On Adaptive Control (in Polish). Central School of Planning and Statistics, Warsaw 1986.

RNDr. Monika Boschková, matematicko-fyzikální fakulta University Karlovy (Faculty of Mathematics and Physics — Charles University), Sokolovská 83, 186 00 Praha 8. Czechoslovakia.