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PŘEDBĚŽNÁ SDĚLENÍ

TWO-STRIP RHEOLOGICAL MODEL FOR SIMPLE ORTHOTROPIC VISCOELASTIC BODIES

[PRELIMINARY COMMUNICATION]

ZDENĚK SOBOTKA

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The complexity of the two-dimensional rheological behavior of anisotropic viscoelastic bodies needs, in some cases, a special representation. Therefore, the author has introduced the two-dimensional rheological models, of which the two-strip model on Fig. 1 for orthotropic viscoelastic bodies is the most simple. It consists of the Hookean elastic zone *H* and the Newtonian viscuous zone *N*. In the direction of the *x*-axis, it behaves like a Kelvin solid and in the direction of the *y*-axis like a Maxwell liquid.

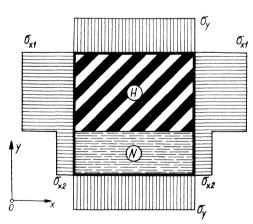


Fig. 1. Two-Strip Rheological Model for a Viscoelastic Body.

The stress σ_x is decomposed into the component σ_{x1} acting in the σ_{x1} elastic zone and into σ_{x2} acting in the viscous zone.

The normal strain rates at the plane-stress state are given by

(1)
$$\frac{\mathrm{d}\varepsilon_x}{\mathrm{d}t} = \frac{1}{E_x} \left(\frac{\mathrm{d}\sigma_{x1}}{\mathrm{d}t} - \mu_x \frac{\mathrm{d}\sigma_y}{\mathrm{d}t} \right) =$$
$$= \frac{1}{\lambda_x} \left(\sigma_{x2} - v_x \sigma_y \right),$$

(2)
$$\frac{\mathrm{d}\varepsilon_{y}}{\mathrm{d}t} = \frac{1}{E_{y}} \left(\frac{\mathrm{d}\sigma_{y}}{\mathrm{d}t} - \mu_{y} \frac{\mathrm{d}\sigma_{x1}}{\mathrm{d}t} \right) + \frac{1}{\lambda_{y}} \left(\sigma_{y} - v_{y} \sigma_{x2} \right),$$

where λ_x , λ_y are the coefficients of normal viscosity,

 μ_x , μ_y the elastic Poisson ratios,

 v_x , v_y the viscuous Poisson ratios.

Introducing $\sigma_{x2} = \sigma_x - \sigma_{x1}$ into (1),

(3)
$$\frac{\mathrm{d}\sigma_{x1}}{\mathrm{d}t} + \frac{E_x}{\lambda_x}\sigma_{x1} = \frac{E_x}{\lambda_x}(\sigma_x - v_x\sigma_y) + \mu_x \frac{\mathrm{d}\sigma_y}{\mathrm{d}t},$$

and hence

(4)
$$\sigma_{x1} = e^{-(E_x t/\lambda_x)} \left\{ \int_0^t \left[\frac{E_x}{\lambda_x} (\sigma_x - \nu_x \sigma_y) + \mu_x \frac{d\sigma_y}{d\tau} \right] e^{E_x \tau/\lambda_x} d\tau + \sigma_{x10} \right\}.$$

Substituting (4) into (1) and performing the integration, one obtains

(5)
$$\varepsilon_x = e^{-(E_x t/\lambda_x)} \left[\int_0^t \left(\frac{\sigma_x - v_x \sigma_y}{\lambda_x} + \frac{\mu_x}{E_x} \frac{d\sigma_y}{d\tau} \right) e^{E_x \tau/\lambda_x} d\tau + \frac{\sigma_{x10}}{E_x} \right] - \frac{\mu_x}{E_x} \sigma_y,$$

i.e.

(6)
$$\varepsilon_x = e^{-(E_x t/\lambda_x)} \left\{ \int_0^t \frac{1}{\lambda_x} \left[\sigma_x - (\mu_x + v_x) \sigma_y \right] e^{E_x \tau/\lambda_x} d\tau + \frac{\sigma_{x10}}{E_x} \right\},$$

which also represents the solution of the following first-order linear differential equation

(7)
$$\lambda_x \frac{\mathrm{d}\varepsilon_x}{\mathrm{d}t} + E_x \varepsilon_x = \sigma_x - (\mu_x + \nu_x) \sigma_y,$$

corresponding to the rheological equation of a Kelvin solid.

Introducing

(8)
$$\sigma_{x1} = E_x \varepsilon_x + \mu_x \sigma_y,$$

obtained from (1), into (2), one obtains, after integration,

(9)
$$\varepsilon_{y} = \frac{1 - \mu_{x}\mu_{y}}{E_{y}} \sigma_{y} - \frac{\mu_{y}E_{x}}{E_{y}} \varepsilon_{x} + \frac{1}{\lambda_{x}} \int_{0}^{t} \left[\left(1 + \mu_{x}v_{y} \right) \sigma_{y} - v_{y}\sigma_{x} + v_{x}E_{x}\varepsilon_{x} \right] d\tau.$$

After substituting from (6), this equation becomes

$$\begin{split} \varepsilon_y &= \frac{1 - \mu_x \mu_y}{E_y} \, \sigma_x \, - \frac{\mu_y E_x}{E_y} \, e^{-(E_x t/\lambda_x)} \left\{ \int_0^t \frac{1}{\lambda_x} \left[\sigma_x - \left(\mu_x + \nu_x \right) \sigma_y \right] e^{E_x \tau/\lambda_x} \, \mathrm{d}\tau \, + \frac{\sigma_{x10}}{E_x} \right\} \, + \\ &+ \frac{1}{\lambda_x} \int_0^t \! \left(\left(1 + \mu_x \nu_y \right) \sigma_y - \nu_y \sigma_x + \nu_y E_x \, e^{-(E_x \tau/\lambda_x)} \! \left\{ \int_0^\tau \frac{1}{\lambda_x} \left[\sigma_x - \left(\mu_x + \nu_x \right) \sigma_y \right] \right. \\ &\cdot e^{E_x \tau/\lambda_x} \, \mathrm{d}\tau \, + \, \frac{\sigma_{x10}}{E_x} \right\} \right) \mathrm{d}\tau \, . \end{split}$$

From (7)

(11)
$$\sigma_x = E_x \varepsilon_x + \lambda_x \frac{\mathrm{d}\varepsilon_x}{\mathrm{d}t} + (\mu_x + \nu_x) \sigma_y ;$$

introducing this into (9) yields after differentiation,

(12)
$$\frac{\mathrm{d}\sigma_{y}}{\mathrm{d}t} + \frac{(1 - v_{x}v_{y})E_{y}}{(1 - \mu_{x}\mu_{y})}\sigma_{y} = \frac{E_{y}}{1 - \mu_{x}\mu_{y}} \left[\frac{\mathrm{d}\varepsilon_{y}}{\mathrm{d}t} + \left(\frac{\mu_{y}E_{x}}{E_{y}} + \frac{v_{y}\lambda_{x}}{\lambda_{y}} \right) \frac{\mathrm{d}\varepsilon_{x}}{\mathrm{d}t} \right],$$

corresponding to the rheological equation of a Maxwell liquid; hence

$$(13) \quad \sigma_{y} = e^{-C_{y}t} \left\{ \frac{E_{y}}{1 - \mu_{x}\mu_{y}} \int_{0}^{t} \left[\frac{\mathrm{d}\varepsilon_{y}}{\mathrm{d}\tau} + \left(\frac{\mu_{y}E_{x}}{E_{y}} + \frac{v_{y}\lambda_{x}}{\lambda_{y}} \right) \frac{\mathrm{d}\varepsilon_{x}}{\mathrm{d}\tau} \right] e^{C_{y}\tau} \,\mathrm{d}\tau + \sigma_{y0} \right\},$$

i. e.

(14)
$$\sigma_{y} = \frac{E_{y}}{1 - \mu_{x}\mu_{y}} \left[\varepsilon_{y} + \left(\frac{\mu_{y}E_{x}}{E_{y}} + \frac{v_{y}\lambda_{x}}{\lambda_{y}} \right) \varepsilon_{x} \right] - \left(\frac{E_{y}}{1 - \mu_{x}\mu_{y}} \right)^{2} \frac{1 - v_{x}v_{y}}{\lambda_{y}} e^{-C_{y}t} \int_{0}^{t} \left[\varepsilon_{y} + \left(\frac{\mu_{y}E_{x}}{E_{y}} + \frac{v_{y}\lambda_{x}}{\lambda_{y}} \right) \varepsilon_{y} \right] e^{C_{y}\tau} d\tau + \sigma_{y0}e^{-C_{y}t},$$

where $C_y = (1 - v_x v_y) E_y / (1 - \mu_x \mu_y) \lambda_y$ is the reciprocal relaxation time.

Substituting (14) into (11) yields

(15)
$$\sigma_{x} = E_{x}\varepsilon_{x} + \frac{(\mu_{x} + \nu_{x}) E_{y}}{1 - \mu_{x}\mu_{y}} \left[\varepsilon_{y} + \left(\frac{\mu_{y}E_{x}}{E_{y}} + \frac{\nu_{y}\lambda_{x}}{\lambda_{y}} \right) \varepsilon_{x} \right] + \lambda_{x} \frac{d\varepsilon_{x}}{dt} - (\mu_{x} + \nu_{x}) .$$

$$\cdot \left(\frac{E_{y}}{1 - \mu_{x}\mu_{y}} \right)^{2} \frac{1 - \nu_{x}\nu_{y}}{\lambda_{y}} e^{-C_{y}t} \int_{0}^{t} \left[\varepsilon_{y} + \left(\frac{\mu_{y}E_{x}}{E_{y}} + \frac{\nu_{y}\lambda_{x}}{\lambda_{y}} \right) \varepsilon_{x} \right] e^{C_{y}\tau} d\tau + \sigma_{y0} e^{-C_{y}t} .$$

The assumption of full compactness of the two-strip model yields, for the symmetrical shear stress and strain, the following expression

(16)
$$\sigma_{xy} = \sigma_{yx} = G\varepsilon_{xy} + \eta \frac{\mathrm{d}\varepsilon_{xy}}{\mathrm{d}t}.$$

If however, the vertical boundaries of the model on Fig. 1 are free to deflect, the body behaves at the vertical shear like a Kelvin solid and the shear stress σ_{xy} is given by (16); for the horizontal shear, the equation of the Maxwell liquid is valid

(17)
$$\frac{\mathrm{d}\sigma_{yx}}{\mathrm{d}t} + \frac{G}{\eta}\sigma_{yx} = G\frac{\mathrm{d}\varepsilon_{yx}}{\mathrm{d}t}$$

from which

(18)
$$\sigma_{yx} = e^{-(Gt/\eta)} \left(\int_0^t G \frac{\mathrm{d}\varepsilon_{yx}}{\mathrm{d}\tau} e^{G\tau/\eta} \,\mathrm{d}\tau + \sigma_{yx0} \right).$$

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